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COMPUTER PROGRAM DEVELOPMENT AND USER'S MANUAL FOR PROGRAM PARACH

By Hughlen I. Murphree Systems Dynamics Laboratory

September 1979

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George C. Marshall Space Flight Center Marshall Space Flight Center, Alabama

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program operational on the Upperating instructions for it used to study the interaction terminal descent. Operating and limitations, and output dare also listed and explained	are included. Program PA dynamics of a parachute and instructions, required inputate ata are described. Subrout	RACH has been extensively d its payload during ut data, program options
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Computer Program Development and User's Manual for Program PARACH

I. INTRODUCTION

This user's manual furnishes complete documentation on Program PARACH, a digital simulation currently being used to investigate the interaction dynamics of a parachute-spent Solid Rocket Booster (SRB) during terminal descent. Program PARACH is written in Fortran and is operational on the Univac 1108 and EMR 6050 computers. The EMR 6050 is used because of the graphic display capabilities of the computer.

Section II presents a discussion of the mathematical model and a summary of resulting equations, while Section III furnishes a description of the program's subroutines. Section IV is a listing of input variables used in the program and their definitions. Finally, Section V gives a program flow chart and a listing of the program.

II. MATHEMATICAL MODEL

The math model simulates a SRB with two parachutes attached at different points on the SRB. Runs made up to now only use one parachute. The other one is zeroed out.

Assumptions - Several assumptions are made to simplify the 3 dimensional math model formulation and its implementation into a digital computer simulation called Program PARACH. These are:

- . All bodies are considered as rigid bodies,
- . The mass and aerodynamic forces of the suspension lines are neglected,
- The center of pressure and center of volume for the parachute canopy are assumed to be located at the center of mass of the canopy material.

Parachute Configuration - The program regards the parachute configuration as a rigid body. It has six degrees of freedom; three translational and three rotational. The main disturbance is due to aerodynamic forces and moments. Use of chute apparent mass and inertia properly distinguishes the parachute from a conventional rigid body.

Booster Configuration - This program also regards the booster as a rigid body. It has six degrees of freedom, 3 translational and 3 rotational. There are aerodynamic forces and moments computed on this rigid body.

System Configuration - The system configuration considers the three rigid bodies to be joined by frictionless attachments that transmit no moments. The attach point constraint relationships are formed by requiring the inertial velocities of the bodies to be the same at the attach point.

Atmospheric Mass Density - Density is calculated using the following equation: $\rho = K * EXP (A_0 + A_1 Z + A_2 Z^2 + A_3 Z^3 + A_4 Z^4 + A_5 Z^5)$. The capability to use a constant density and omit the equation is also available.

Parachute and Payload Drag - Drag is a function of velocity, mass density of air, angle-of-attack, reference area, and other factors. Wake effects on either body were not considered.

Rotational Damping Coefficient - The damping on payload and parachute due to rotational velocities is currently set to zero. However, the program includes the provisions to include the rotational damping derivatives.

Retro Thrusters on the Payload - The program has the capability of having eight retro-rockets on the payload, positioned and skewed as desired. There can be more if the appropriate dimension statements are enlarged. At ignition, each thruster follows the thrust profile in the THR table.

Wind Model

Table Look-Up (Subroutine TBL) - A wind table is used as an alternative to a programmed wind profile. The wind table uses subroutine TBL which is an interpolation scheme. The subroutine is used in every other table look-up in this program.

Parachute Side Force - Side forces are considered in this program as part of the parachute dynamics. It is presented here as a function of the angle-of-attack (see figure 1).

Program Equations - The following program equations are computed, accounting for inertial, reaction, gravity, aerodynamic, and thruster forces. The program equations are computed for both the booster and the parachute yielding both translational and rotational accelerations and the sum of the forces acting on the two bodies.

$$\hat{\Omega} = M^{-1} (F(I) + F(R) + F(A) + F(C) + F(G))$$

Where: $M^{-1} = an 18 \times 18$ diagonal matrix whose elements are the mass and inertia values for the SRB and the two parachutes.

 $F^{(1)}$ = Inertial Forces and Moments (18 x 1 vector) $F^{(R)}$ = Reaction Forces and Moments (18 x 1 vector)

 $F^{(A)}$ = Aerodynamic Forces and Moments (18 x 1 vector)

 $F^{(C)}$ = Control Forces and Moments (18 x 1 vector)

 $F^{(G)}$ = Gravity Forces and Moments (18 x 1 vector)

$$\mathbf{\Omega}^{T} = (U_{1}, V_{1}, W_{1}, P_{1}, Q_{1}, R_{1}, U_{2}, V_{2}, W_{2}, P_{2}, Q_{2}, R_{2}, U_{3}, V_{3}, W_{3}, P_{3}, Q_{3}, R_{3})$$

The following equations are used to compute the Inertial Forces and Moments $(F^{(1)})$.

$$F^{(I)} = \begin{vmatrix} F_1^{(I)} \\ I_1 \\ I_1 \\ F_2^{(I)} \\ I_2 \\ I_3 \\ I_1^{(I)} \\ I_2 \\ I_3 \\ I_4 \\ I_5 \\ I_5 \\ I_6 \\ I_7 \\ I_8 \\ I_8$$

Where:

$$F_{i}^{(T)} = -M_{i} \Omega_{i} V_{i}$$

$$L_{i}^{(T)} = -M_{i} \Omega_{i} V_{i}$$

$$L_{i}^{(T)} = -\Omega_{i} I_{i} \Omega_{i}$$

$$L_{i}^{(T)} =$$

and: V_i , V_i , W_i are the linear velocities of the respective bodies, M_i is the mass term and P_i , Q_i , R_i are the angular velocities of the respective bodies.

Coordinate Transformations:

i = 1, 2, 3

The general transformation between any two Euclidean coordinate systems is written in terms of Euler parameters (quaternions) as:

$$G_{\mathbf{i}} = \begin{bmatrix} (q_{1}^{\mathbf{i}})^{2} - (q_{2}^{\mathbf{i}})^{2} - (q_{3}^{\mathbf{i}})^{2} + (q_{4}^{\mathbf{i}})^{2} \\ 2 (q_{1}^{\mathbf{i}} q_{2}^{\mathbf{i}} - q_{3}^{\mathbf{i}} q_{4}^{\mathbf{i}}) \\ 2 (q_{1}^{\mathbf{i}} q_{3}^{\mathbf{i}} + q_{2}^{\mathbf{i}} q_{4}^{\mathbf{i}}) \\ 2 (q_{1}^{\mathbf{i}} q_{2}^{\mathbf{i}} + q_{3}^{\mathbf{i}} q_{4}^{\mathbf{i}}) \\ 2 (q_{2}^{\mathbf{i}} q_{3}^{\mathbf{i}} - q_{1}^{\mathbf{i}} q_{4}^{\mathbf{i}}) \\ 2 (q_{2}^{\mathbf{i}} q_{3}^{\mathbf{i}} - q_{1}^{\mathbf{i}} q_{4}^{\mathbf{i}}) \\ - (q_{1}^{\mathbf{i}})^{2} - (q_{2}^{\mathbf{i}})^{2} + (q_{3}^{\mathbf{i}})^{2} + (q_{4}^{\mathbf{i}})^{2} \end{bmatrix}$$

Where:

$$G_1$$
 (transformation from inertial to SRB frame) G_2 (transformation from inertial to parachute A frame) G_3 (Transformation from inertial to parachute B frame) $G_1^2 = G_2 \ G_1^T$ (transformation from SRB to parachute $G_1^3 = G_3 \ G_1^T$ (transformation from SRB to parachute B)

 $$\operatorname{\textsc{The}}\ q\mbox{'s}$ in the coordinate transformation matrices are quaternions given by the following equations:

$$q_{1}^{i} = \sin \frac{\varphi_{i}}{2} \cos \frac{\psi_{i}}{2} \cos \frac{\theta_{i}}{2} - \sin \frac{\psi_{i}}{2} \sin \frac{\theta_{i}}{2} \cos \frac{\varphi_{i}}{2}$$

$$q_{2}^{i} = \sin \frac{\theta_{i}}{2} \cos \frac{\psi_{i}}{2} \cos \frac{\varphi_{i}}{2} + \sin \frac{\psi_{i}}{2} \sin \frac{\varphi_{i}}{2} \cos \frac{\theta_{i}}{2}$$

$$q_{3}^{i} = \sin \frac{\psi_{i}}{2} \cos \frac{\theta_{i}}{2} \cos \frac{\varphi_{i}}{2} - \sin \frac{\theta_{i}}{2} \sin \frac{\varphi_{i}}{2} \cos \frac{\psi_{i}}{2}$$

$$q_{4}^{i} = \cos \frac{\psi_{i}}{2} \cos \frac{\theta_{i}}{2} \cos \frac{\varphi_{i}}{2} + \sin \frac{\psi_{i}}{2} \sin \frac{\theta_{i}}{2} \sin \frac{\varphi_{i}}{2}$$

Where $\theta_{\mathbf{i}}$, $\phi_{\mathbf{i}}$, and $\psi_{\mathbf{i}}$ are the Euler angles

i = 1 refers to the SRB

i = 2 refers to parachute A

i = 3 refers to parachute B

The differential equation governing the evolution of the quarternions as a function of time is given by:

$$\begin{vmatrix} \dot{q}_{1}^{i} \\ \dot{q}_{2}^{i} \\ \dot{q}_{3}^{i} \\ \dot{q}_{4}^{i} \end{vmatrix} = \begin{vmatrix} 0 & -R_{i} & Q_{i} & -P_{i} \\ R_{i} & 0 & -P_{i} & Q_{i} \\ -Q_{i} & P_{i} & 0 & -R_{i} \\ P_{i} & Q_{i} & R_{i} & 0 \end{vmatrix} \cdot \begin{vmatrix} q_{1}^{i} \\ q_{2}^{i} \\ q_{3}^{i} \\ q_{4}^{i} \end{vmatrix}$$

Likewise, the Gravity Forces and Moments $(F^{(G)})$ are derived from the following:

$$\mathbf{F}^{(G)} = \begin{bmatrix} \mathbf{F}_{1}^{(G)} \\ \mathbf{0} \\ \mathbf{F}_{2}^{(G)} \\ \mathbf{0} \\ \mathbf{F}_{3}^{(G)} \\ \mathbf{0} \end{bmatrix}$$

Where:
$$F_{\mathbf{i}}^{(G)} = \begin{bmatrix} 0 \\ G_{\mathbf{i}} \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ m_{\mathbf{i}} g \end{bmatrix}$$

 $\mathbf{m_{i}}$ is the appropriate actual mass term

g is the gravitational force

The thrust vector due to retro-rockets is computed using the following equations

Where: THR(t) is the thrust profile as a function of time (t).

DCOSX(i), DCOSY(i), and DCOSZ(i) are the direction cosines of the thrust vector.

XR(i), YR(i), ZR(i) are the moment
arms of the retro-rockets.

The aerodynamic forces and moment vectors are computed using the following equations:

$$F^{(A)} = \begin{vmatrix} F_1^{(A)} \\ L_1^{(A)} \\ F_2^{(A)} \\ L_2^{(A)} \\ F_3^{(A)} \\ L_3^{(A)} \end{vmatrix}$$

Where:

$$f_{i}^{(A)} = \begin{vmatrix} f_{xi} \\ f_{yi} \\ f_{zi} \end{vmatrix}$$
 and $L_{i}^{(A)} = \begin{vmatrix} L_{i} \\ M_{i} \\ N_{i} \end{vmatrix}$

Define:

$$f_{xi} = -\frac{1}{2} \rho v^{2} S C_{N(i)} \frac{\tilde{U}_{i}}{(\tilde{U}_{i}^{2} + \tilde{V}_{i}^{2})^{\frac{1}{2}}}$$

$$f_{yi} = -\frac{1}{2} \rho v^{2} S C_{N(i)} \frac{\tilde{V}_{i}}{(\tilde{U}_{i}^{2} + \tilde{V}_{i}^{2})^{\frac{1}{2}}}$$

$$f_{zi} = \frac{1}{2} \rho v^{2} S C_{A(i)}$$

$$L_{i} = \frac{1}{2} \rho v^{2} S \mathcal{L} C_{M(i)} \frac{\tilde{V}_{i}}{(\tilde{U}_{i}^{2} + \tilde{V}_{i}^{2})^{\frac{1}{2}}}$$

$$M_{i} = -\frac{1}{2} \rho v^{2} S \mathcal{L} C_{M(i)} \frac{\tilde{U}_{i}}{(\tilde{U}_{i}^{2} + \tilde{V}_{i}^{2})^{\frac{1}{2}}}$$

$$N_{i} = 0.0$$

 $\mathbf{v}^2 = (\mathbf{v}_i^2 + \mathbf{v}_i^2 + \mathbf{w}_i^2)$

S = Reference Area (May be computed as a function of time (reefing))

= Reference Length

The calculation of the reaction force is quite a bit more complicated as far as computational procedures are concerned and is given by the following equations

$$F^{(R)} = T_1 (F^{(I)} + F^{(A)} + F^{(C)} + F^{(G)}) + T_2 \cdot \Omega$$

Where:

$$T_{1} = (-B^{T} K^{-1}) (BM^{-1})$$

$$T_{2} = -B^{T} K^{-1} B$$

$$K = BM^{-1} B^{T}$$

$$B = \begin{bmatrix} G_{1}^{2} & G_{1}^{2} & \tilde{L}_{1} & -E_{3} \tilde{L}_{A_{1}} & 0 & 0 \\ G_{1}^{3} & -G_{1}^{3} & \tilde{L}_{2} & 0 & 0 & -E_{3} \tilde{L}_{B_{1}} \end{bmatrix}$$

$$\tilde{L}_{1} = \begin{bmatrix} 0 & -\tilde{L}_{1}z & \tilde{L}_{1}y \\ \tilde{L}_{1}z & 0 & \tilde{L}_{1}x \\ -\tilde{L}_{1}y & \tilde{L}_{1}x & 0 \end{bmatrix}$$

$$\tilde{L}_{A1} = \begin{bmatrix} 0 & -\tilde{L}_{A1}z & \tilde{L}_{A1}y \\ \tilde{L}_{A1}z & 0 & \tilde{L}_{A1}x \\ -\tilde{L}_{A1}y & \tilde{L}_{A1}x & 0 \end{bmatrix}$$

$$\tilde{L}_{B1} = \begin{bmatrix} 0 & -\tilde{L}_{B1}z & \tilde{L}_{B1}y \\ \tilde{L}_{B1}z & 0 & \tilde{L}_{B1}x \\ -\tilde{L}_{B1}y & \tilde{L}_{B1}x & 0 \end{bmatrix}$$

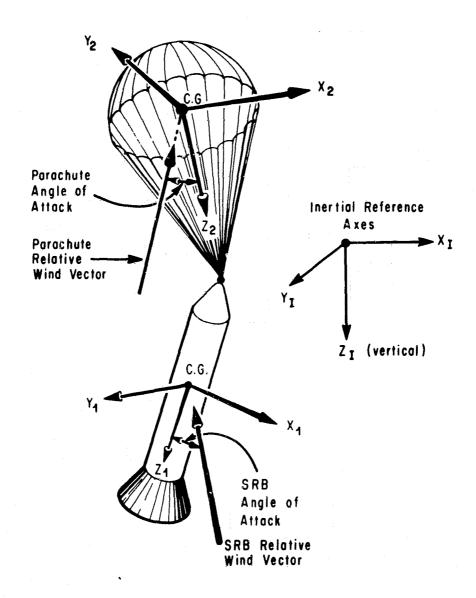


FIG. 1. PROGRAM COORDINATE SYSTEMS

III. PROGRAM SUBROUTINES

Subroutine: RUNGE

Purpose: Subroutine RUNGE is a subroutine used to integrate the

differential equations and produces a table of integrated

values.

Use: RUNGE (KUTTA, TIME, DT, NVAR, NDVAR)

Description of Parameters:

KUTTA - is a control integer (controls the number of times through integration loop)

TIME - is time of integration

DT - is the time increment

NVAR - is the number of variables to be integrated once

NDVAR - is the number of variables to be integrated twice

Remarks: Fourth-order RUNGE-KUTTA

Subroutine: TBL

Purpose: This subroutine provides a linear interpolation between data

points in a tabular function of one variable.

Use: TBL (X, Y, X1, N, Y1)

Description of Parameters:

X - is the independent variable

Y - is the dependent variable

Xl - is the X argument

N - is the number of data points in the table

Y - is the result desired

Remarks: The X array of data must be in ascending order.

Subroutine: LINSYS

Purpose: This subroutine takes the inverse of a matrix.

Use: LINSYS (A, NROWSA, NCOLSA, DET, B, ARRAY)

Description of Parameters:

A - is the array containing the coefficients of the linear system.

NROWSA - is the number of rows of the square Matrix A.

NCOLSB - is the number of columns of the Matrix B in the equation A*X = B.

DET - is the determinate of Matrix A

B - is the Matrix B = A*X

NARRAY - is the number of rows of the arrays in which A and B are stored in the calling program.

Subroutine: XTAN 2

Purpose: This subroutine is used to define correct quadrant.

Use: XTAN 2 (A, B)

Description of Parameters:

A - is the value of the numerator of the angle.

B - is the value of the denominator of the angle.

IV. INPUT PARAMETERS

FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
X1	x_1	R	Inertial Location of SRB CG in the x Direction
Y1	$\mathbf{Y_1}$	R	Inertial Location of SRB CG in the y Direction
Z1	^z 1	R	Inertial Location of SRB CG in the z Direction
U1	$\mathbf{v_1}$	R	Inertial Velocity of the SRB CG in the x Direction
V1	v_1	R	Inertial Velocity of the SRB CG in the y Direction
W1	$\mathbf{w_1}$	R	Inertial Velocity of the SRB CG in the z Direction
X2	x ₂	R	Inertial Location of Parachute A CG in the x Direction
Y2	Y ₂	R	Inertial Location of Parachute A CG in the y Direction
Z2	^Z 2	R	Inertial Location of Parachute A CG in the z Direction
U2	^U 2	R	Inertial Velocity of Parachute A CG in the x Direction
V2	v_2	R	Inertial Velocity of Parachute A CG in the y Direction
W2	W ₂	R	Inertial Velocity of Parachute A CG in the z Direction

Note: Any consistent set of units may be used.

FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
х3	x ₃	R	Inertial Location of Parachute B CG in the x Direction
Y3	Y ₃	R	Inertial Location of Parachute B CG in the y Direction
Z3	z ₃	R	Inertial Location of Parachute B CG in the z Direction
N	N	I	(9) Number of Data Points in Table
N1	N_1	I	(41) Number of Data Points in Table
U3	u ₃	R	Inertial Velocity of Parachute B CG in the x Direction
V3	$\mathbf{v_3}$	R	Inertial Velocity of Parachute B CG in the y Direction
w3	w ₃	R	Inertial Velocity of Parachute B CG in the z Direction
P1	\mathbf{P}_{1}	R	Angular velocity of SRB About the xl Axis
Q1	Q_1	R	Angular velocity of SRB About the yl Axis
R1	R ₁	R	Angular velocity of SRB About the zl Axis
THI1	e_1	R	2nd Euler Angle of SRB
PHI1	ϕ_1	R	3rd Euler Angle of SRB
PSI1	ψ_1	R	1st Euler Angle of SRB
P2	P ₂	R	Angular Rotation of Parachute A about the x2 Axis

FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
Q2	Q_2	R	Angular volocity of Parachute A About the y2 Axis
R2	R ₂	R	Angular velocity of Parachute A About the z2 Axis
THI2	θ2	R	2nd Euler Angle of Parachute A
PHI2	Ø ₂	R	3rd Euler Angle of Parachute A
PSI2	ψ_2	R	lst Euler Angle of Parachute A
Р3	P ₃	R	Angular velocity of Parachute B About the x3 Axis
Q3	Q ₃	R	Angular velocity of Parachute B About the y3 Axis
R3	R ₃	R	Angular velocity of Parachute B About the z3 Axis
THI3	θ_3	R	2nd Euler Angle of Parachute B
PHI3	ϕ_3	R	3rd Euler Angle of Parachute B
PS13	ψ_3	R	lst Euler Angle of Parachute B
XIX1	$^{\mathtt{I}}_{\mathtt{x}_{1}}$	R	Moment of Inertia About $x_1 Axis$ of SRB
XIY1	¹ y ₁	R	Moment of Inertia About y_1 Axis of SRB
XIZ1	1 ₂₁	R	Moment of Inertia About z_1 Axis of SRB
XIX2	$\mathbf{I_{x_2}}$	R	Moment of Inertia About x_2 Axis of Parachute A

FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
XIY2	$\mathbf{I}_{\mathbf{y}_2}$	R	Moment of Inertia About y_2 Axis of Parachute A
XIZ2	$\mathbf{I_{z}}_{2}$	R	Moment of Inertia About z_2 Axis of Parachute A
XIX3	$\mathbf{I_{x_3}}$	R	Moment of Inertia About x_3 Axis of Parachute B
XIY3	$\mathbf{I}_{\mathbf{y}_3}$	R	Moment of Inertia About y ₃ Axis of Parachute B
XIZ3	$\mathtt{I_{z_3}}$	R	Moment of Inertia About z ₃ Axis of Parachute B
S1	s_1	R	Surface Area of SRB
S2	s_2	R	Surface Area of Parachute A
S 3	s_3	R	Surface Area of Parachute B
YL	1	R	Reference Diameter of SRB
YPL	2	R	Reference Diameter of Parachute A
YPL3	3	R	Reference Diameter of Parachute B
xxw2	M_{1g}	R	Weight of Parachute A
xxw3	M _{2g}	R	Weight of Parachute B
XM1	\mathtt{M}_{1}	R	*Mass of SRB
XM21	M_{x2}	R	*Mass of Parachute A in x Direction
XM22	M _{y2}	R	*Mass of Parachute A in y Direction
XM23	M _{z2}	R	*Mass of Parachute A in z Direction

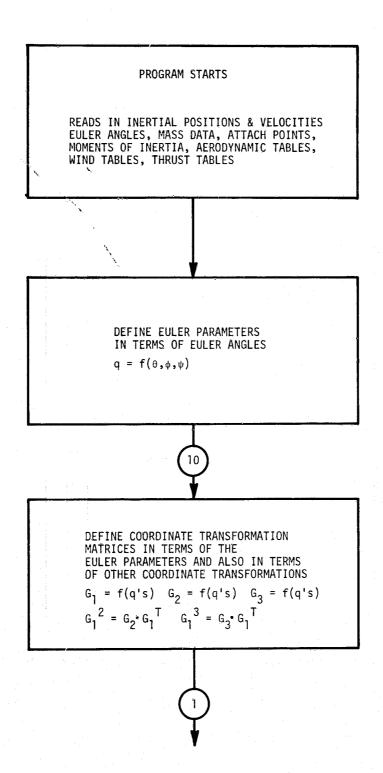
^{*} Mass is equal to total mass plus apparent mass

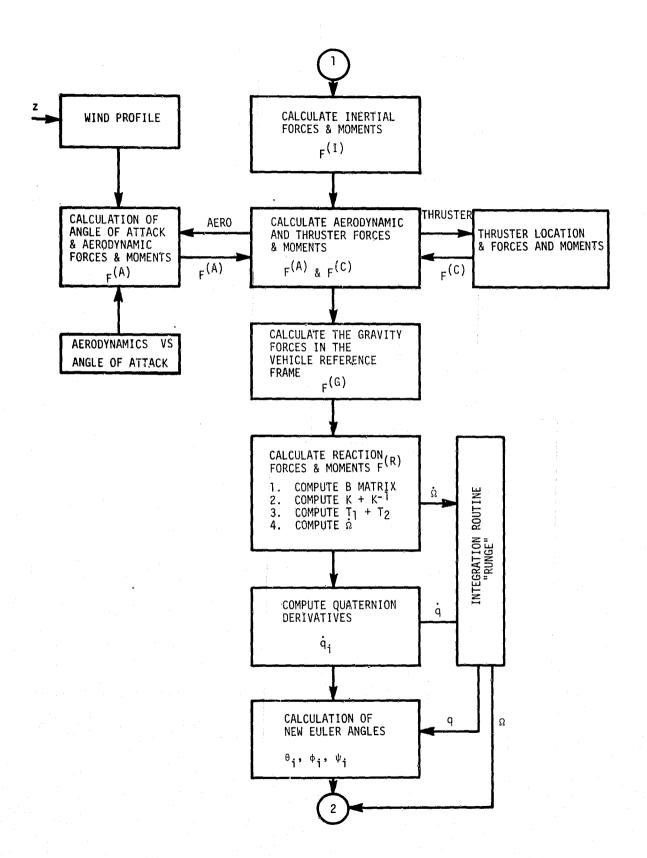
FØRTI MNEMO		ENGINEERING SYMBOLS	TYPE	DEFINITIONS
X	M31	M _{x3}	R	Mass of Parachute B in x Direction
XI	M32	My3	R	Mass of Farachute B in y Direction
XI	M33	^M z3	R	Mass of Parachute B in z Direction
G		g	R	Gravity
X	LX1	L _{×1}	R	xl Distance From CG of SRB to Attach Point of Parachute A
X	LY1	L _{y1}	R	yl Distance From CG of SRB to Attach Point of Parachute A
X	LZ1	$^{ m L}{_{ m z}}{_{ m 1}}$	R	zl Distance From CG of SRB to Attach Point of Parachute A
X	LX2	L _{x2}	R	xl Distance From CG of SRB to Attach Point of Parachute B
X	LY2	L _{y2}	R	yl Distance From CG of SRB to Attach Point of Parachute B
х	LZ2	L _{z2}	R	zl Distance From CG of SRB to Attach Point of Parachute B
X	LAX1	$\mathbf{L}_{\mathbf{x}\mathbf{A}}$	R	x2 Distance From Attach Point to CG of Parachute A
Х	LAY1	L _{yA}	R ,	y2 Distance From Attach Point to CG of Parachute A
Х	KLAZ1	$\mathtt{L}_{\mathbf{z}\mathbf{A}}$	R	z2 Distance From Attach Point to CG of Parachute A
X	KLBX1	$\mathtt{L}_{\mathbf{x}\mathtt{B}}$	R [x3 Distance From Attach Point to CG of Parachute B

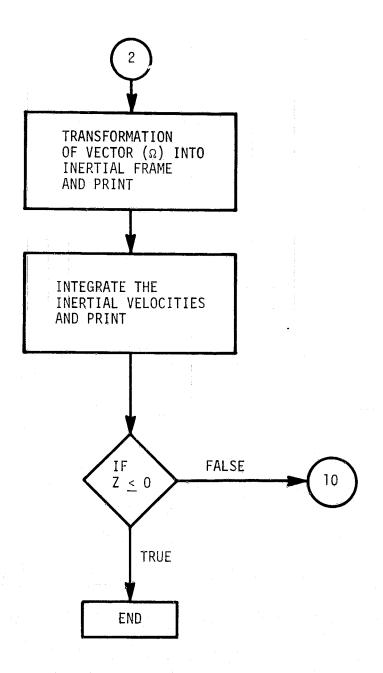
FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
XLBX1	$\mathbf{L}_{\mathbf{x}\mathbf{B}}$	R	y3 Distance From Attach Point to CG of Parachute B
XLBY1	$^{\mathrm{L}}$ yB	R	z3 Distance From Attach Point to CG of Parachute B
XLBZ1	$\mathbf{L}_{\mathbf{z}\mathbf{B}}$	R	Direction Cosines of the Eight Retro-Rockets (I = 1,8)
DCOSX(I)	D cos x(i)	R	Direction Cosines of the Eight Retro-Rockets (I = 1,8)
DCOSY(I)	D cos y(i)	R	Direction Cosines of the Eight Retro-Rockets (I = 1,8)
DCOSZ(I)	D cos z(i)	R	Distance From CG of SRB to Retro- Rockets
LCX(I)	x(i)	R	Distance From CG of SRB to Retro- Rockets
LCY(I)	y(i)	R	Distance From CG of SRB to Retro-Rockets
TIMX(I)	t	R	Time Table
THR(I)	$\mathtt{T_{hr}}$	R	Thrust Table
Z(I)	Z	R	·Altitude Table
UWD(I)	$\mathbf{u}_{\mathbf{w}}$	R	u Wind Table
VWD(I)	$v_{\mathbf{w}}$	R	v Wind Table
AL(I)	α	R	Alpha Table
FCNA1(I)	$^{\rm c}$ N $_{\!lpha 1}$	R	Table of Aerodynamic Forces Acting or SRB (Normal)

FØRTRAN MNEMONIC	ENGINEERING SYMBOLS	TYPE	DEFINITIONS
FCAAL(I)	$c_{A_{\alpha 1}}$	R	Table of Aerodynamic Forces Acting or SRB (Axial)
FCMA1(I)	$^{\mathrm{c}}_{^{\mathrm{M}}\!\alpha 1}$	R	Table of Aerodynamic Forces Acting or SRB (Moment)
FCNA2(I)	$^{ m c}_{ m N}\!_{ m c2}$	R	Table of Aerodynamic Forces Acting on Parachute A (Normal)
FCAA2(I)	$c_{A_{\alpha_2}}$	R	Table of Aerodynamic Forces Acting on Parachute A (Axial)
FCMA2(I)	c _M α2	R	Table of Aerodynamic Forces Acting on Parachute A (Moment)
FCNA3(I)	$c_{N_{\alpha 3}}$	R	Table of Aerodynamic Forces Acting on Parachute B (Normal)
FCAA3(I)	$c_{A_{\alpha 3}}$	R	Table of Aerodynamic Forces Acting on Parachute B (Axial)
FCMA3(I)	c _M a3	R	Table of Aerodynamic Forces Acting on Parachute B (Moment)

V. FLOW CHART AND PROGRAM LISTING







Graphics Display for "PARACH" (Sample Results)

The following plots were made on the ERR-6050 computer. These are included to illustrate the graphics display capability of the computer.

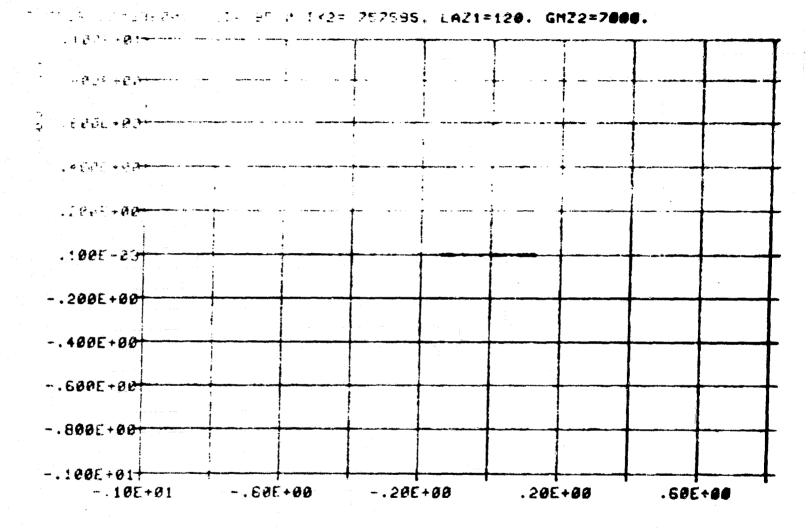
The curves shown are representative results for one parachute with the appropriate parachute characteristics listed at the top of each graph.

9-19/755RFC2=39800. H2I= 85.0 IX2= 758888. LAZ1=120. GMZ2=7000.

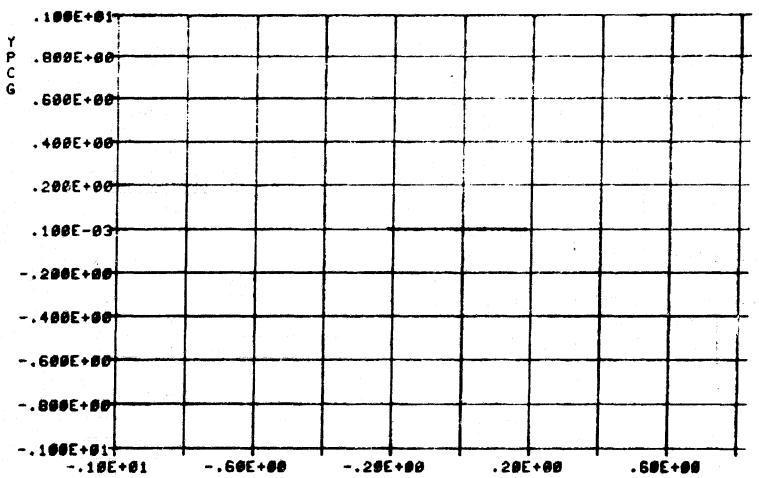








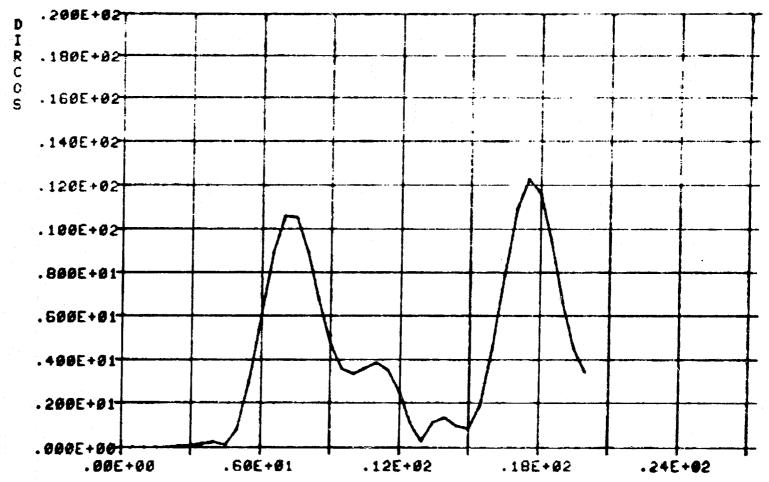




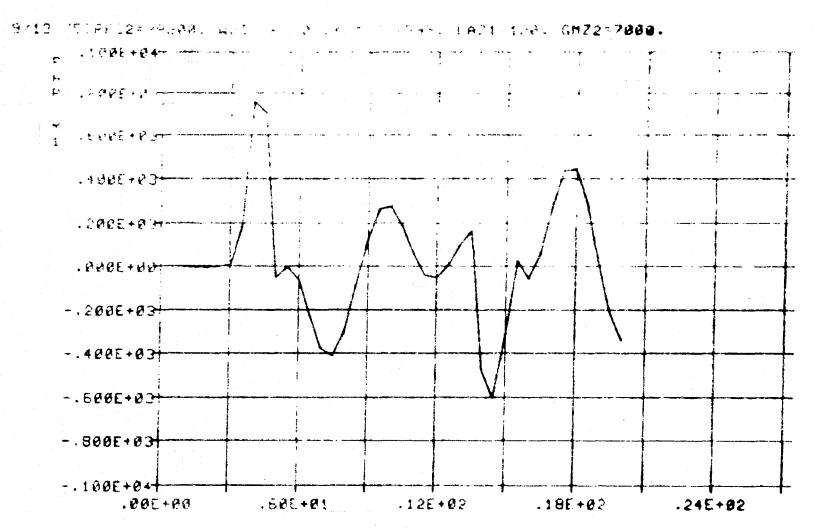
XPCG

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9/19/75SRFC2=39800. W2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.

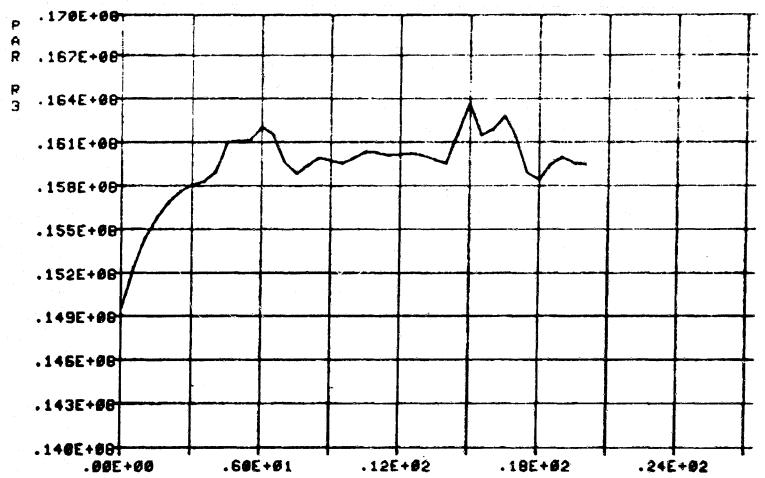


TIME

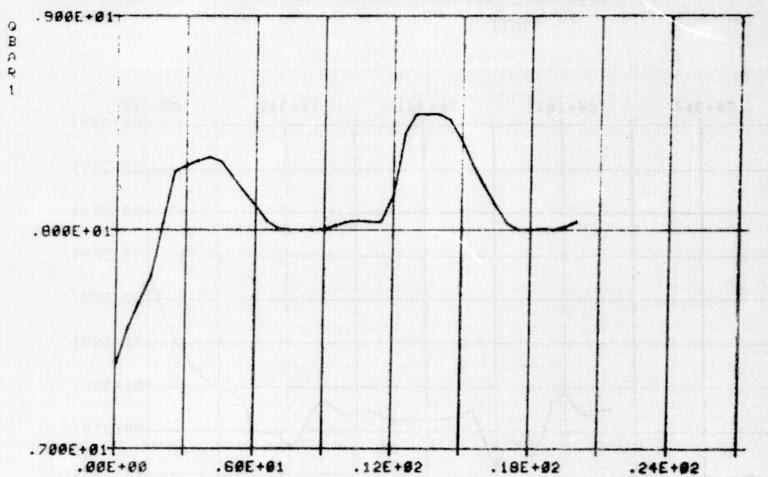


TIME

3/19/755RFC2=39800. H2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.

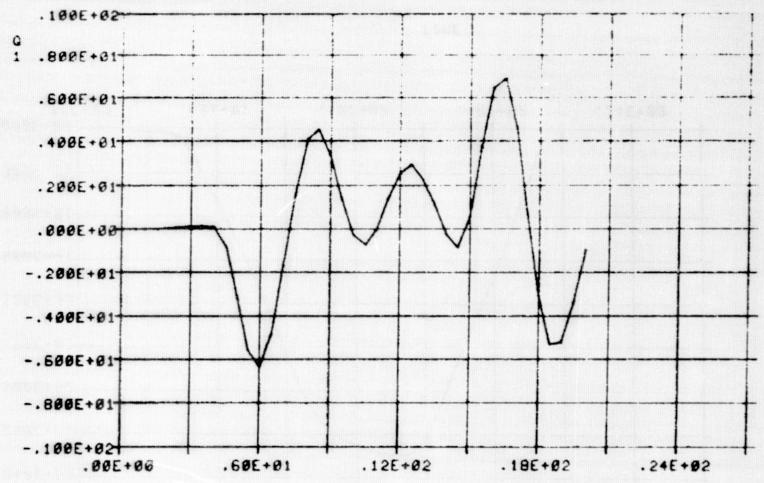


9/19/75SRFC2=39800. W2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7600.

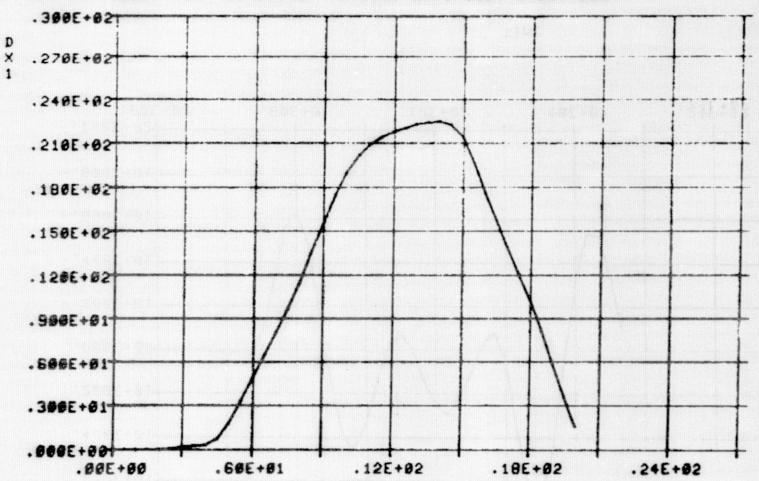


TIME

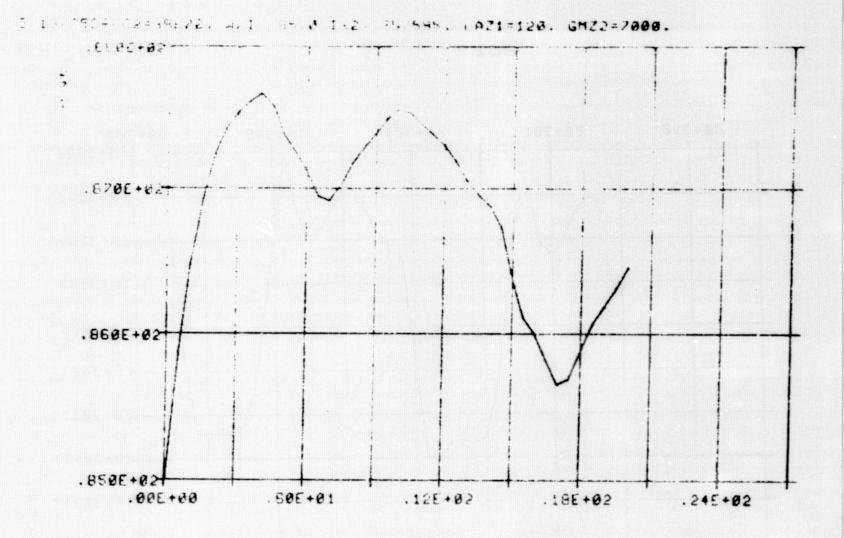
3/19/75SRFC2=39800. H21= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.



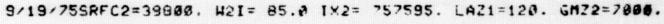
9/19/75SRFC2=39800. H2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.

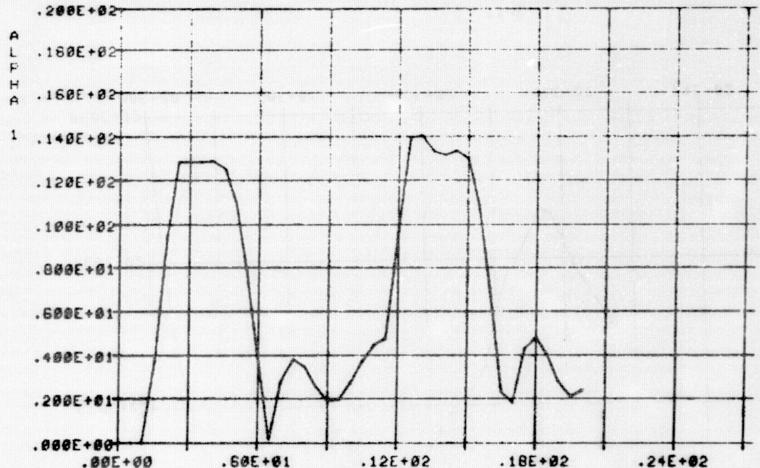


TIME

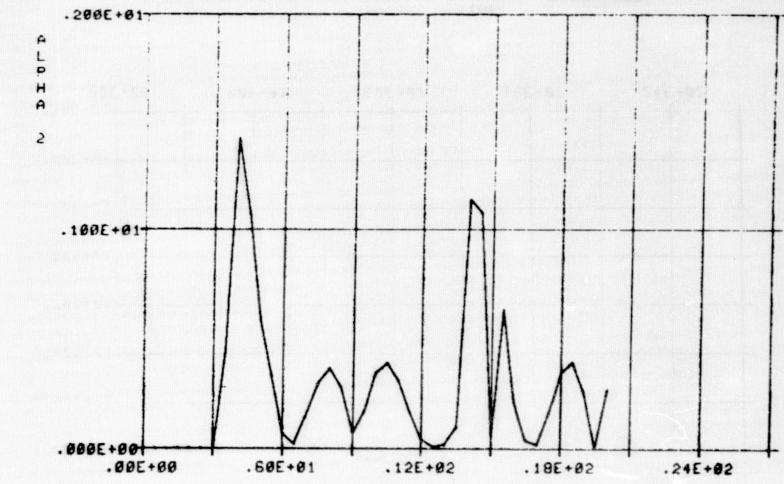


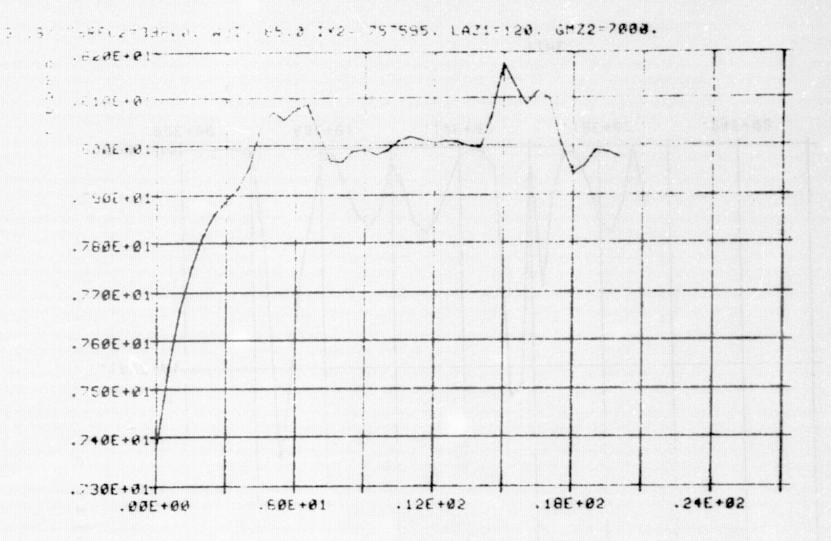
TIME





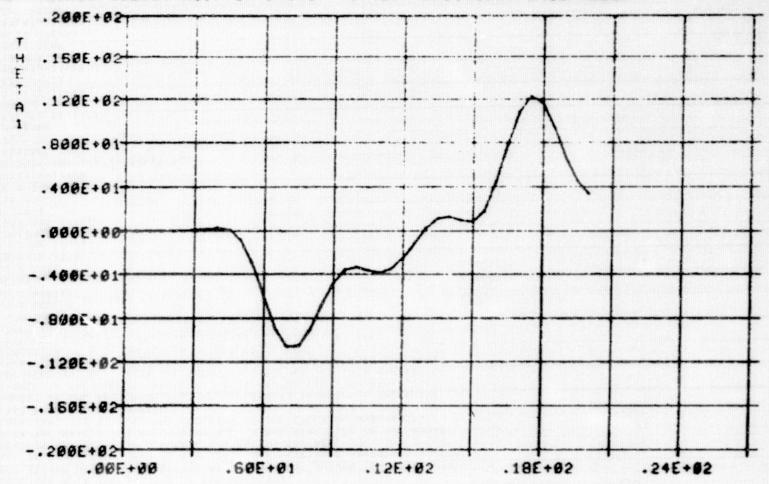
9/13/755RFC2=39800. W2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.





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9/19/75SRFC2=39800. H2I= 85.0 IX2= 757595. LAZ1=120. GMZ2=7000.



TIME

HYBI	NZU6+TPF	\$(0).LINSYS	
1		SUBROUTINE LINSYS(A,NROWSA,NCOLSB,DET,B,NARRAY)	
2	C	A IS THE ARRAY CONTAINING THE COEFFICIENTS OF THE LINEAR SYSTEM.	A STATE
3	C	NRONSA IS THE NUMBER OF ROMS FOR COLUMNS OF THE SQUARE MATRIX A.	
	C	THAT IS. A IS AN NROWSA BY NROWSA MATRIX.	
5	Č	NCOLSB IS THE NUMBER OF COLUMNS OF THE MATRIX B IN THE EQUATION	
6	C	A+X = 8.	
	HALLING SHEET HIS HOLD IN		
7	C	THAT IS, THIS ROUTINE MAY BE USED TO SOLVE THE ABOVE EQUATION	
8	C	WHEN B (AND X) ARE EITHER SINGLE VECTORS OR SEVERAL VECTORS	
9	C	CONJOINED IN A MATRIX. NOTE THAT IE B IS A UNIT MATPIX. THE	
10	C	SOLUTION X IS THE INVERSE OF THE MATRIX A.	
11	C	DET IS THE DETERMINANT OF THE MATRIX A. DET SHOULD BE CHECKED TO	
2	C	SEE IF IT IS ZERO, FOR IN THIS CASE THE MATRIX IS SINGULAR AND THE	
3	C	RESULTS RETURNED ARE MEANINGLESS, EXCEPT FOR DET.	
10	C	B IS THE MATRIX WHICH CONTAINS THE RIGHT HAND SIDE OF THE ABOVE	
2	C	EQUATION. IT IS ALSO THE LOCATION OF THE SOLUTION MATRIX, X, ON	
6	Č	EXIT FROM THE SUBROUTINE.	
7	č	NAKRAY IS THE NUMBER OF RONS OF THE ARRAYS IN WHICH A AND B ARE	
8	C	STORED IN THE CALLING PROGRAM. THIS MAY BE EQUAL TO NROWSA.	
9	č	BUT NEED NOT BE. THUS THE USER MAY STORE A(1.J) IN A LARGER	
C	C	ARRAY THAN IS STRICTLY NECESSARY. THIS IS USEFUL WHEN THE EXACT	_
1	c	나 보고 있다면 하나 나는 사람들이 되었다. 나는 사람들이 살아보고 살아보고 살아보고 살아보고 살아보고 살아보고 살아보고 살아보고	
2		DIMENSION OF A IS UNKNOWN AT COMPILATION TIME.	
		INTEGER Z1, Z2, Z3, Z4, Z5, Z6, Z7, Z8, Z9, Z10, Z11, Z12, Z13, Z14	
3		DIMENSION A(1),8(1)	
		N = NROWSA	
5		NN = NCOLSB	
6		NK = NARRAY	
7		DET=1. IJ100050	
b		DO 2 K=1,N	
9		Z1=K+(K-1)+NK	
		IF(K-N) 30,3,30	
1	36	CONTINUE	
12		TEST=ABS (A(Z ₁))	
3		KP1=K+1	
14		L=K	
15		DO 4 1=KP1+N	
6		72=I+(K-1)*NK	
17		IF (TEST-ABS (A(Z2)))31,4,4	
8	31	TEST=ABS (A(ZZ))	
9		L=1	
0	4	CONTINUE	
1		IF(L-K) 41,3,41	
2	41	00 5 J = K,N	
	41		
3		Z3=L+(J-1)*NK	
4		TEMP=A(25)	
5		Z4=K+(J-1)+NK	
6		A(Z3)=A(Z4)	
7	5	A(Z4)=TEMP	
P		DO 15 J=1,NN	
9		Z5=L+(J-1)+NK	
0		TEMP=8(25)	A LIFE
1		Z6=K+(J-1)*NK	
2		B(25)=B(26)	-
3	15	B(Z6)=TEMP	
		DET = -DET	
5	3	DET=DET*A(Z1)	
/ 100	T	A(21)=1./A(21)	-

LINS	YS		DATE 040379	PAGE
57		IF(K-N) 35,19,35		
58	35	DO 6 J = KP1.N		
59		Z7=K+(J-1)+NK		
60		A1271=A1271+A1211		
61	6	CONTINUE		
62	19	00 16 J=1,NN		
63		Z9=K+(J-1)+NK		
64	16	B(Z9)=B(Z9)*A(Z1)	20003807	
₩ 65		DO 7 I=1,N		
REPRODUCIBILITY		Z1C=I+(K-1)+NK		
67		IF(I-K) 160,7,160		
₹ 68 <u></u>	160	FAC=A(Z1D)		
9 69		DO 8 J=KP1.N		
2 70		Z11=I+(J-1)+NK		
Ö 71		Z12=K+(J-1)*NK		
H 72		E=A(Z11)		
₩ 73		D=E-FAC+A(212)		
C 79		1F(1.DE-9*ABS (E)-ABS (D))162.161.161		
75	161	D = C.		
K 76	162	A(Z11)=D		
	8	CONTINUE		
Q 77		DO 18 J = 1,NN		
. 79		Z13=I+(J-1)*NK		
79 80 81		Z14=K+(J-1)*NK		
81	18	B(Z13)=B(Z13)-FAC*B(Z14)		
82	7	CONTINUE		
83	2	CONTINUE		
84		RETURN		
85		END		
HDG,P	MAIN			
PRI,S	MAIN P3DF 3 2 S	L73R1 04/03/79 18:29:28		
		275 0 20 1000		
· · · · · · · · · · · · · · · · · · ·				
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PAIN		DATE 040379 PAGE 2
57	EQUIVALENCE (FA(17,1),YM3),(FA(18,1),YN3),	
58	And the state of t	0380
59		10390
60		00400
61	1(FA(13,1),FX3),(FA(14,1),FY3),(FA(15,1),FZ3),(FA(16,1),YL3), MOOC 1(FG(1,1),FG1(1,1)),(FG(2,1),FG1(2,1)),(FG(3,1),FG1(3,1)),	00410
63	1(FG(7,1),FG2(1,1)),(FG(8,1),FG2(2,1)),(FG(9,1),FG2(3,1)),	
64	1(FG(13,1),FG3(1,1)),(FG(14,1),FG3(2,1)),(FG(15,1),FG3(3,1)).	
65	1(FI(1.1),FII(1.1)),(FI(2.1),FII(2.1)),(FI(3.1),FII(3.1)),	
66	1(FI(7,1),F21(1,1)),(FI(8,1),F21(2,1)),(FI(9,1),F21(3,1)),	
67	1(F1(13,1),F31(1,1)),(F1(14,1),F31(2,1)),(F1(15,1),F31(3,1)).	
68	1(FI(4.1), XL1I(1,1)), (FI(5,1), XL1I(2,1)), (FI(6,1), XL1I(3,1)),	
69	1(F1(10,1), xL21(1,1)), (F1(11,1), xL21(2,1)), (F1(12,1), xL21(3,1)),	
70	1(F1(16,1),XL31(1,1)),(F1(17,1),XL31(2,1)),(F1(18,1),XL31(3,1))	
71	EQUIVALENCE (V1M(1,1),U1),(V1M(2,1),V1),(V1M(3,1),W1) EQUIVALENCE (V2M(1,1),U2),(V2M(2,1),V2),(V2M(3,1),W2)	
73	EQUIVALENCE (V3M(1,1),U3),(V3M(2,1),V3),(V3M(3,1),W3)	
79	EQUIVALENCE (XOM11(2,1),Q1),(XOM11(3,1),R1),	
75	1 (XOM21(2,1),Q2),(XOM21(3,1),R2),	
76	2 (X0m31(2.1),03),(X0M31(3,1),R3)	
77	DATA PFRL7/6HPAR R1,11+6H /	
78	DATA PFRL8/6HPAR R2,11+6H	
79	DATA PFRL9/6HPAR R3,11*6H /	
80	DATA PS2L/6HS2 ,11*6H /	
81	DATA POBAIL/6HQBAR1 ,11*6H /	
82	DATA PQBAZL/6HQBARZ ,11*6H / DATA PZZL/6HZ2 ,11*6H /	
84	DATA PP1L/6HP1 ,11+6H /	
85	DATA PQ1L/6HQ1 ,11*6H /	
86	DATA PRIL/6HR1 ,11*6H /	
87	DATA PDX1L/6HDX1 ,11+6H /	
88	DATA PDY1L/6HDY1 ,11*6H /	
89	DATA PDZ1L/6HDZ1 ,11*6H /	
90	DATA PALIL/6HAL1 ,11*6H /	
91	DATA PALZL/6HAL2 +11*6H /	
93	DATA TIMEL/6HTIME 11*6H /	
94	DATA (THR (I), I=1,9)/0.,39400.,39400.,0.,0.,0.,0.,0.,0.,0.,	
95	DATA (AL(I),I=1,15)/0.,10.,20.,30.,40.,50.,60.,70.,80.,90.,	
96	*100.,110.,120.,130.,150./	
97	DATA(DCOSX(I) ,I = 1,8)/8*u./	
98	DATA(DCOSY(1) ,1 = 1,8)/8+0./	The state of the s
99	DATA(DCOSZ(I) ,I = 1,81/8*-1./	
106	DATA (LCX (1),1=1,8)/8*.2/	
101	DATA (LCY (I),I=1,8)/8*.G/ DATA (LCZ (I),I=1,8)/8*.G/	
103	DATA (FCAA2(I), I=1,15)/.55,.525,.475,.385,.275,0.,0.,0.,0.,0.,0.,	
164	*0.,0.,0.,0./	
165	DATA (FCNA2(1), I=1,15)/005,.125,.19,.25,10*.3/	
106	DATA (FCMA2(1), 1=1,15)/0.,025,0625,095,125,10*15/	
107	DATA (ZCAA(I),I=1,15)/.75,1.25,1.75,2.35,2.35,2.0,1.5,0.85,0.22,	
108	*25,25,.5,.22,15,75/	
109	DATA (ZCNA(1), I=1,15)/0.0,.5,1.5,3.1,5.4,7.4,8.2,6.4,6.,6.,6.,6.,	
110	*7.6,7.6,3,2/	
111	DATA (ZCMA(I), I=1,15)/0.0,1.8,3.,3.3,4.7,6.7,8.0,6.0,1.7,-2.5,	
112	DATA (ZCAA(I), I=16,30)/1.35,1.5,1.9,2.5,2.45,2.0,1.5,.9,.35,1,	
	Park 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	

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114	*3,.4,.25,1,75/		
15	DATA (ZCNA(1),1=16,30)/0.0,0.5,1.6,3.7,6.,8	8.,9.4,10.2,10.8,11.2,	
16	+11.0.10.4,9.8,8.4,4.0/		
17	DATA (ZCHA(I), I=16,30)/0.0,1.6,2.8,3.0,3.6,	6.8,8.2,4.0,-2,8,-7,0,	
18	*-10.7,-12.4,-13.0,-11.8,-4.7/		
19	DATA (ZCNA(1),1=31,45)/0.,.7,2.,4.1,7.5,10.	7,13.,14.25,15.8,16.,	
20	*15.6.14.7.14.4.11.5.4.5/		
21	DATA (ZCHALI), 1=31,45)/0.1.8.2.3.3.4.5.7.7	7.3.7.8.5.3.0.,-6.,-11.7	
22	*,-17.,-20.7,-19.1,-8./		
23	DATA (ZCAA(I), I=31,45)/1.25,1.7,2.,2.2,2.,1	1.65.1.0525456	
24	*.5,25,25,45,9/		
25	DATA (WD(1),1 = 1,41)/56.3,56.7,55.1,53.	6.52.1.50.8.49.5.48.2	
	146.8,45.2,43.4,41.1,38.8,36.6,34.5,32.4,31.	2 20 1 26 6 24 0 19.5	
26	146.8,45.2,43.4,41.1,38.8,38.8,34.3,32.4,31.	-77- 7- 7- 7- 7- 1- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7- 7-	
21	213.5.5.812.41.721.525.22728.7.		
28	3-38.,-40.,-41.7,-43.5,-45.8,-48.1,-50.4,-0.	.07	
29	DATA (FCNA3(1), 1=1,15)/15+0./		
30	DATA (FCMA3(1),1=1,15)/15+0./		
31	DATA (FCAA3(1).1=1.15)/15*0./	700 700 700 0	
32	DATA (Z(I), I=1,41)/-35000.,-3900.,-3800.,-3	3700.,-3600.,-3200.0,	
33	1-3400.0,-3300.0,-3200.0,-3100.0,-3000.0,-25	900.6,-2800.0,-2700.0,	
34	2-2600.0,-2500.0,-2400.0,-2300.0,-2200.0,-21	100.0,-2000.0,-1900.0,	
35	3-1800.0,-1700.0,-1600.0,-1500.0,-1400.0,-13	300.0,-1200.0,-1100.0	
36	4-1000.0,-900.0,-800.0,-700.0,-600.0,-500.0,	,-400.0,-300.0,-200.0,	
37	5-100.0.0.0/		
38	DATA (TIMX(I),I=1,9)/0.0,0.2,4.2,4.4,5.0,6.	.0,7.0,8.0,40.0/	
39	DATA (PERAL 211), I=1,12)/0.1.217.385.525.	.685,1.,0.,5.,10.,15.,	
40	*25.,40./		
41	DATA (ZCAA2(I), I=1,12)/6+0.,.119,.14,.135,.		
42	DATA (ZCNAZ(I), I=1,12)/6+0.,0.,.03,.055,.08		
143	DATA (ZCHAZ(1), 1=1,12)/6+0., 0.,035,06	65,1,2,28/	
44	DATA (ZCAA2(I), I=13,24)/.212,.225,.225,.223	3,.21,.16,.289,.3,.325,	
145	*.325,.3,.2/		
146	DATA (ZCNA2(I), I=13,24)/0.,.03,.071,.115,.2	2,.27,.0,.028,.064,.11,	
147	*.185,.27/		
148	DATA (ZCHA2(1),1=13,24)/0.,04,08,13,-	23,31,0.,033,075	
149	*,13,22,31/		
15C	DATA (ZCAA2(1),1=25,36)/.377,.395,.415,.415	5,.39,.32,.55,.55,.55,.5	
51	*4,.50,.41/		
52	DATA (ZCNA2(1), 1=25, 36)/0., .02, .052, .095, .1	175,.275,.0,.01,.032,.09	
53	*, .17, .28/		
54	DATA (ZCMA2(1),1=25,36)/0.,02,06,115,	2295.001303	
55	*7,091,175,28/		
56	DO 609 I=1,18	M0000440	
57	J=1	M0000450	
58	FC(1,J)=0.0		
59	609 CONTINUE	MD000480	
60	NH=0		
	AA0=1.3302117E-02		
162	AA1=-8.8502064E-U5		
163	AA2=-4.2143056E-U9		
164	AA3=5.9517557E-13		
	AA4=-3.9744789E-17		
165	AA5=7.8771273E-22		
166	14대 NED 2014 (1914년) 2014 전 12 12 12 12 12 12 12 12 12 12 12 12 12		
167	TPR=0.0		
168	READ 3, (N,N1,N2)		
169	READ 1, (RAPP, RETR, ZMRP1, ZMRP2, NPARA)		

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171	READ 1, (DT, DELP)					
172	PRINT 1,(DT,DELP)					
173	READ 1, (X1, Y1, Z1, U1, V1, W1)					
174	READ 1, (x2, y2, Z2, U2, V2, W2)					
175	READ 1, (X3, Y3, Z3, U3, V3, W3)					
176	READ 1,4P1,Q1,R1,TH11,PH11,PS11)	THE RESERVE THE RESERVE THE PARTY OF THE PAR				
177	READ 1, (P2, Q2, R2, THI2, PHI2, PSI2)					
178	P1=P1/57•3					
179	Q1_Q1/57.3					THE RES
180	R1=R1/57.3					
181	P2=P2/57.3					
162	Q2-Q2/57·3					
183	R2=R2/57.3					
184	IHI1=THI1+0.01744					
185	THI2=THI2+0.01744					
186	pHI1=PHI1*0.01744					
187	PH12=PH12*0.01744					
188	PSI1=PSI1*u.01744					
189	PSI2=PSI2*0.01744					
190	READ 1. (P3.Q3.R3.THI3.PHI3.PSI3)					
191	READ 1, (XIX1, XIY1, XIZ1, S1, YL, XM1) .					
192	READ 1. (XIX2D. XIY2D. XIZZ . STZ, YPL, XXWZ)					
193	READ 1, (XIX3, XIY3, XIZ3, S3, YPL3, XXW3)					
194	READ 1. (XLX1.XLY1.XLZ1.XLAX1.XLAX1.XLAZ1)					
195	READ 1, (XLX2, XLY2, XLZ2, XLBX1, XLBY1, XLBZ1)					
196	READ 1, (XM21T, XM22T, XM23T, XM31, XM32, XM33)					
197	READ 1,1G,RALPH)					
198	PRINT 3, (N, N1, N2)					
199	PRINT 1,(X1,Y1,Z1,U1,V1,W1)					
200	PRINT 1,(X2,Y2,Z2,U2,V2,W2)					
261	PRINT 1,(X3,Y3,Z3,U3,V3,W3)					
262	PRINT 1,(P1,Q1,R1,THI1,PHI1,PSI1)					
203	PRINT 1,(P2,Q2,R2,TH12,PH12,PS12)					
264	PRINT 1,(P3,Q3,R3,THI3,PHI3,PSI3)					
205	PRINT 1, (XIX1, XIY1, XIZ1, S1, YL, XM1)					
206	PRINT 1,(XIX2D,XIY2D,XIZ2 ,ST2,YPL,XXW2)					
207	PRINT 1,4X1X3,X1Y3,X1Z3,S3,YPL3,XXW3)					
208	PRINT 1, (XLX1, XLY1, XLZ1, XLAX1, XLAY1, XLAZ1)					
209	PRINT 1,(XLX2,XLY2,XLZ2,XLBX1,XLBY1,XLBZ1)					
210	PRINT 1, (XM21T, XM22T, XM23T, XM31, XM32, XM33)					
211	PRINT 1.(G)					
212	3 FORMAT (312)					
213	2 FORMAT (5E15.6)	M0001030				
219	1 FORMAT (6E12.6)					
215	XMAAL(1)= .4					
216	XMAAL(2) = .6					
217	XMAAL(3) = .9					
218	DO 550 I = 4,18					
719	550 XMAAL(I) = AL(I-3)					
220	NAZ(1) = 3					
21	NAZ(2) = 15					
22	NSZ(1) = -1	PARTIES - DESCRIPTION OF STREET				
23	NSZ(2) = -1					
24	KAPP = .245					
25	PoRo=15.0			CHEST SALE	strate a	
26	POR0=16.2					

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28	KOV2 = 1.	
29	K093 = 1.	
3C	x2FR = x2	
31	Y2PR = Y2	_
32	ZZPR = ZZ	
33	1111 = 0	_
34	1112 = 0	
35	NAZZ(1) = 6	_
36	NAZZ(2) = 6	
37	N5Z2(1) = -1	-
36	NS22(2) = -1	
39	SS ₀ = •1	-
40	\$50=0.0	
41	\$\$0=.01	
42	551 = .7	
43	SS1=0.75	
44	\$\$1=1.0	
45	\$\$1=0.8	-
46	552 = 1.	
47		-
48	111=8.0	
49	111=12.0	
50	112 = 20.	
51	Sp101 = .55+\$12	-
52	TEMPO = .65 * PORO * YPL	
53	CP1=0.0	-
54	CP2=0.0	
55	CP3=0.0	
56 57	CP4=0.0 CP5=0.0	
58	CP6=0.0	
59	DO 744 I=1.8	
PL .	CP1=CP1+DC0SX(1)	
61	CP2=CP2+DCOSY(1)	
62	CP3=CP3+DC0SZ(I)	-
63	CP4=CP4+(LCY(I)+DCOSZ(I)-LCZ(I)+DCOSY(I))	
64	CP5=CP5+(LCZ(I)+DCOSX(I)-LCX(I)+DCOSZ(I))	
65	CP6=CP6+(LCX(I)+DCOSY(I)-LCY(I)+DCOSX(I))	
66	744 CONTINUE	
67	Q11=SIN(PHI1/2.)*COS(PSI1/2.)*COS(THI1/2.)-SIN(PSI1/2.)*SIN(THI1/2H0001050	
68	*.)*C0S(PHI1/2.) H0001060	
69	Q12=SIN(PH12/2.)+COS(PS12/2.)+COS(TH12/2.)-SIN(PS12/2.)+SIN(TH12/2M0001070	
71	*.)*C0S(PH12/2.) M0001080	
71	Q13=S1N(PH13/2.)+COS(PS13/2.)+COS(TH13/2.)-S1N(PS13/2.)+S1N(TH13/2M0001090	
72	+.)+COS(PHI3/2.) MODO1100	
73	Q21=SIN(THI1/2.)+COS(PSI1/2.)+COS(PHI1/2.)+SIN(PSI1/2.)+SIN(PHI1/2HOOD1110	ATT
74	*.)*COS(THI1/2.) MOUDI120	H
75	422=SIN(TH12/2.)*COS(PS12/2.)*COS(PH12/2.)*SIN(PS12/2.)*SIN(PH12/2M0001130	
76	. +.)+COS(THI2/2.) MODD1140	
17	423=SIN(TH13/2.)*COS(PS13/2.)*COS(PH13/2.)*SIN(PS13/2.)*SIN(PH13/2M0001150	
78	+.)+COS(THI3/2.)	
79	Q31=SIN(PSI1/2.)*COS(THI1/2.)*COS(PHI1/2.)*SIN(THI1/2.)*SIN(PHI1/2MD001170	
33	*.)*COS(PSI1/2.)	
81	Q32=SIN(PS12/2.)+COS(TH12/2.)+COS(PH12/2.)+SIN(TH12/2.)+SIN(PH12/2M0001190	
67	+.1*C0S(PSI2/2.) MOUD1200	
	Q33=SIN(PSI3/2.)*COS(THI3/2.)*COS(PHI3/2.)-SIN(THI3/2.)*SIN(PHI3/2MOUC1210	

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785	Q41=COS(PSI1/2.)*COS(THI1/2.)*COS(PHI1/2.)*	SIN(PS11/2.1+SIN(THI1/2M0001230				
286	*.)*SIN(PHI1/2.)	H0001240				
	Q42=COS(PS12/2.)*COS(THI2/2.)*COS(PHI2/2.)*	SIN(pSI2/2.)*SIN(THI2/2M0001250				
287 288 289 290 291 292 293 294 295 296 296 297 298 299	*.)*SIN(PHI2/2.)	M0001260	and the second			
289	Q43=COS(PSI3/2.)+COS(THI3/2.)+COS(PHI3/2.)+	SIN(PSI3/2.)*SIN(THI3/2M0001270				
290	*.)*SIN(PHI3/2.)	MD00128D				102111
201	NFQ=30	MD0 _{D1} 290				
H 292	NSO=0	M0001300				
293	1=0.0	M0001320				
C 294	11=i	M0001330				
H 295	TIME = 0.	MOUD1340				
H 296	DELT-DT					
297	DO 78 I=1,3	M0001360				
298	DO 78 J=1.3	M0001370				
299	E3(1,J):0.0	M0001380				
O 300	78 CONTINUE	M0001390				
9 300 301	E3(1,1)=1.0	MD001400				
	E3(2,2)=1.0	MDQD1410				
302 303 304	£3(3,3)=1.0	MD001420				
303	XL1(1,1)=0.0	MD001430				
305	X _L 1(1,2)=-XLZ1	MODD1440				
306		M0001450				
	XL1(1,3)=XLY1	M0001460				
307	XL1(2,1)7XLZ1	M0001470				
308	XL1(2,2)=0.0	M0001480				
309	XL1(2,3)=-XLX1	M0001490				
310	XL1(3,1)=-XLY1	M0001500				
311	XL1(3,2)=XLX1	M0001510				
312	XL1(3,3)=0.0	M0001520				
313	xL2(1,1)=0.0	M0001530				
319	XL2(1,2)=-XLZ2	M0001540				
315	XL2(1,3)=XLY2	M0001550				
316	XL2(2,1)=XL22	M0001560				
317	XL2(2,2)=0.0	MD001570				
318	XL2(2,3)=-XLX2	M0001580				
319	XL2(3,1)=-XLY2	M0001590				
320	XL2(3,2)=XLX2	M0001600			_	
321	X(2(3,3)=0.0					
322	XLA1(1,1)=0.0	M0001610				
323	XLA1(1,2) = -XLAZ1	M0001620				
324	XLA1(1,3)=XLAY1	M0001630				
325	XLA1(2,1)=XLAZ1	M0001640				
326	XLA1(2,2)=0.0	M0001650				
327	XLA1(2,3)=-XLAX1	M0001660				
328	XLA1(3,1)=-XLAY1	M0001670				
329	XLA1(3,2)=XLAX1	M0001680				
330	XLA1(3,3)=0.0	M0001690				
331	XLB1(1,1)=0.0	H0U01700				
332	XLB1(1,2) = -NLBZ1	M0001710				III ST
333	XLB1(1,3)=XLBY1	M0001720				
334	XLB1(2,1)=XLB21	M0001730				
335	XLB1(2,2)=0.0	MOU01740				
336	XLB1(2,3)=-XLBX1	M0001750				
337	xLB1(3,1)=-XLBY1	M0001760				
338	XLB1(3,2)=XLBX1	M0001770				
339	XLB1(3,3)=0.0	M0001780				
340	7LOS CONTINUE	M0001790				
341	xG1(1,1)=0.0	MD001800				HIEROR

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342	xG1(2,1)=0.0	M0001810
343	xG1(3,1)=XH1*G	MODC1820
344	xG2(1,1)=0.0	M0001830
345	XG2(2,1)=0.0	M0001840
346	XG2(3,1) = XXW2	M0001850
397	x63(1,1)=0.0	M000186g
348	XG3(2,1)=0.0	M0001870
349	XG3(3-1) = XXN3	M0001880
350	00 93 1=1,3	M0001890 M0001900
351	D0 93 J=1,3	M0001910
352	B13 ₁ I,J)=-E3(I,J) B14(I,J)=xLA1(I,J)	M0001920
353		M0001930
354 355	B15(I,J)=0.0 B16(I,J)=0.0	M0001940
356	B23(1,J)=0.0	M0001950
357	B24(I.J)=0.0	Mp001960
358	B25(I,J)=-E3(I,J)	M0U01970
359	B26(I,J)=-xLB1(I,J)	M000198
360	BD13(1,J)=0.0	M0001990
361	BD14(1,J)=0.0	M0002000
362	BD15(1,J)=0.0	M0002010
363	BD16(1,J)=0.0	MD002020
364	BD23(1,J)=0.0	M0002030
365	BD24(I,J)=0.0	MOGO2040
366	BD25(I,J)=0.0	M0002050
367	B026(I,J)=0.0	M0002060
368	93 CONTINUE	M0002070
369	D0 7 1=1,3	H0002080
370	DO 7 J=7,9	M0002090
371	B(I,J)=B13(I,J-6)	M0002100
312	80(1,J)=BD13(1,J-6)	M0002110
373	7 CONTINUE	M0002120
374	DO 8 I=1,3	M0002130
375	00 8 J=10,12	M0002140
376	3(I,J)=B14(I,J-9)	M0002150
377	BD(I,J)=BD14(I,J-9)	M0002160
378	8 CONTINUE	M0002170 M0002180
379	00 9 I=1,3	M0002180
380 381	00 9 J=13,15	M0002200
362	B(I,J)=B15(I,J-12) 6D(I,J)=BD15(I,J-12)	M0002210
383	9 CONTINUE	M0002220
384	00 10 1=1,3	M0002230
385	UO 10 J=16,18	MO0D2240
386	B(1,J)=B16(1,J-15)	M0002250
387	1G CONTINUE	M0002270
388	DO 13 I=4,6	M0002280
389	DO 13 J=7,9	M0002290
390	B(1,J)=B23(1-3,J-6)	MOOD2300
391	BD(1,J)=BD23(1-3,J-6)	M0002310
392	13 CONTINUE	M0002320
393	DO 14 I=4.6	M000233g
394	DO 14 J=10,12	MOCO2340
395	B(I,J)=B24(I-3,J-9)	M0002350
396	BD(1,J)=BD24(I-3,J-9)	M0002360
397	14 CONTINUE	M0UC2370
398	DO 15 I=4,6	M0U02380

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399	00 15 J=13,15	MD002390				
LD	B(1,J)=B25(1-3,J-12)	M0002400				
01	BD(I,J)=BD25(I-3,J-12)	M0002410				
02	15 CONTINUE	MD002420				
03	DO 16 I=4,6	M0002430				
04	D0 16 J=16.18	M0002440				
05	B(I,J)=-B26(I-3,J-15)	M0002450				
06	BD(1,J)=BD26(1-3,J-15)	M0002460				
u7	16 CONTINUE	M0002470				
08	00 39 1=1,18	MDD02480				2000
U9	DO 39 J=1,18	M0002490				
1C	M(1,J)=0,	M0002500				
11	39 CONTINUE	M0002510				
12	M11,17=XH1	M0 ₀₀ 25 ₂₀ M0002530				
19	M(2,2)=XM1	M0002540				
15	M(3,3)=XM1	MO002550				
16	M(4,4)=XIX1 M(5.5)=XIY1	M0002560				
17	M(6,6)=XIZ1	M0002570				
18	M(13,13)=XM31	M0002640				
19	M(14,14)=XM32	M0002650				
20	M(15,15)=XM33	M0002660				
21	M(16,16)=XIX3	M0002670				
22	M(17,17)=x1y3	MD002680				
23	M(18,18)=XIZ3	M0002690				
24	00 53 1=1,18	M0002700				
25	00 53 J=1,18	M0002710				
26	M1(I,J)=0.	H0002720				
27	53 CONTINUE	M0002730				
28	MI(1,1)=1.0/XM1	MDD02740				
29	MI(2,2)=1.0/XM1	M0002750				
30	MI(3,3)=1.0/xM1	M0002760				
31	MI(4,4)=1.0/X1X1	M0002770				
32	MI(5,5)=1.0/XIY1	M0002780				
33	MI(6,6)=1.U/XIZ1	M0002790				
34	MI(13,13)=1.0/XM31	MD002860				
35	MI(14,14)=1.0/XM32	M0002870				
36	MI(15,15)=1.0/xM33	MD002880				
37	MI(16,16)=1.0/XIX3	M0002890				
38	MI(17,17)=1.0/XIY3	M0002900				
39	MI(18,18)=1.0/XIZ3	M0002910				
40	D0 51 I=1,3	M0002920				
43	D0 51 J=1,3	M0002930				
42	M1(I,J)=0.0	M0002940				
43	M2(I,J)=0.0	M0002950				
44 45	M3(1,J)=0.0	M0002960				
	51 CONTINUE M1(1,1)=XM1	MDD02970				
4 <u>6</u>	M1(2,2)=XM1	M0002980 M0002990				
48	M1(3,3)=XM1	M0003000				
49	M3(1,1)=XM31	MOD03040				
50	M3(2,2)=XM32	M0003050				
51	M3(3,3)=xM33	M0003060				
52	D ₀ 27 1=1,3	MD003070				
53	0 ₀ 27 J=1,3	M0003070				
4	X11(1,J)=0.0	MDUD3090				
55	X12(1,J)=0.0	10003070				

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456	X13(1,J)=0.0	M0003110				
457	27 CONTINUE	MD003120				
458	x11(1,1)=x1x1	h2003130				
459	XI1(2,2)=XIY1	M0003140				
460	XI1(3,3)=XIZ1	M0003150				
461	x13(1,1)=x1x3	M0003190				
462	X13(2,2)=X1Y3	M0003200				
463	x13(3,3)=x123	M0003210				
464	FG(4,1)=0.0	M0003220				
465	FG(5,1)=0.0	M0003230				
466	FG(6,1)=0.0	M0003240				
967	EG(10.1)=0.0	M0003250				
468	FG(11,1)=0.0	M0003260 M0003270				
469	FG(12,1)=0.0	M0003270				
471	FG(16,1)=0.0	M0003290				
972	FG(17,1)=0.0 FG(18,1)=0.0	M0003300				
473	300 IND=4	MD003310				
474	60 TO 4	M0003320				
475	200 IND=1	M0003330				
476	SUD CONTINUE	MD003340				
477	CALL RUNGE(IND.TIME.DELT.39.0)	M0003350				
478	4 QD11=-(-R1*Q21+Q1*Q31-P1*Q41)*O.5	M0003360				History
479	77=-71*0.3048					
480	RHO=(1.16790729*ExP(AA0+ZZ*(AA1+ZZ*(AA2+ZZ*(AA3+ZZ*(AA4+ZZ*(A	45111				
481	1))))•0.00194					
482	DELD1 = TEMPD * (SQRT(SS1) - SQRT(SS0)) * KOV1					
48?	DELD2 = TEMPD * (SQRT(SS2) - SQRT(SS1)) * KOV2					
484	DELD3 = TEMPD + (1 - SQRT(SS2)) + KOV3					
485	DELISO = DELD1 * DELD1					
486	DEL2SQ = DELD2 * DELD2					
487	DEL3SQ = DELD3 + DELD3					
488	IF (TIME.GE.TT1) GO TO 50U7					
489	XYZPRM = (X2 - X2PR)**2 + (Y2 - Y2PR)**2 + (Z2 - Z2PR)**2 PER = SSU + (SS1 - SSD)*XYZPRM/DEL1SQ					
491	SDDOT = (2,*H2*SDTOT*(SS1-SSD)*SQRT(XYZPRH))/DEL1SQ					
492	IF (PER.LE.SS1) GO TO 7020					
493	PER=\$\$1					
494	SDDOT = D.					
495	60 TO 7020					
496	5u07 IF (SS1.EQ.1) 60 TO 7020					
497	IF (TIME.GE.TT2) GO TO 1070					
498	IF (ITT1.EQ.1) GO TO 6007					
199	X2PR = X2					
500	Y2PR = Y2					
561	Z2PR = Z2					
502	1771 = 1					
563	6UO7 CONTINUE					
564	XYZPRM = 1X2 - X2PR1**2 + 1Y2 - Y2PR1**2 + 1Z2 - Z2PR1**2					
565	PER = SS1 + (SS2 - SS1)*XYZPRM/DEL2SQ					
506	SDDOT = (2.*H2*SDTOT*(SS2-SS1)*SQRT(XYZPRM))/DEL2SQ					
507	IF (PER.LE.SS2) 60 TO 7020					
508	PER=SS2					
509	SDD01 = 0.					
510	60 10 7020					
511	1076 IF (SS2.EQ.1) 60 TO 7020 IF (ITT2.EQ.1) 60 TO 1170					

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513	X2PR = X2	Helicological Control				
514	Y2PR = Y2					
515	Z2PR = Z2					
516	1112 = 1					92250 00100
517	1170 CONTINUE					
518	XYZPRM = (X2 - X2PR)**2 + (Y2 - Y2PR)**2 + (Z2 - Z2PR)**2 PER = SS2 + (1 SS2)*XYZPRM/DEL3SQ					
520	SDDOT = (2.*42*SDTOT*(1SS2)*SQRT(XYZPRM))/DEL3SQ					
521	1F (PER.LE.1.0) Go To 7020					
522	PER=1.0					
523	SDDOT = Q.					
524	7U2U CONTINUE					
525	9905 S2=PER+ST2					
526	SDRAG = PER+SDTOT					
527	RALPHA=RALPH+YPL+(-0.22+PER+D.22)					
528	ZMAPP=RHQ*SDRAG*SQRT(SDRAG)*KAPP/SQRT(NPARA)					
529	XMAPP = (8*PER + 1.2)*ZMAPP					
530	YMAPP = XMAPP					
531	HZDOT = 1.5*RHO*SDDOT*SQRT(SDRAG)*KAPP					
532	XM21=XMAPP+(XXW2/G)					
533 534	XM22=YHAPP+(XXH2/g) XM23=ZMAPP+(XXH2/g)					
535	XIX2=XIX2D+YHAPP*RAPP*RAPP					
536	XIY2=XIY2D+XMAPP+RAPP+RAPP					
537	H(7,7)=XH21	M0002580				
538	M(8,8)=xM22	M0002590				
539	M(9,9)=XM23	M0002600				
540	H(10,10)=XIX2	MD002610				
541	M(11,11)=XIY2	M0002620				
542	M(12,12)=XIZ2	H0002630				
543	MI(7,7)=1.0/XM21	MD002800				
544	MI(8,8)=1.0/xM22	M0002810				
545	MI(9,9)=1.0/XM23	H0002820				
546	MI(10,10)=1.0/XIX2	M0002830				
547	MI(11,11)=1.0/XIY2	M0002840				
549	HI(12,12)=1.0/XIZ2	M0002850				
550	M2(1,1)=XM21 M2(2,2)=XM22	M0003010				
551	M213,3)=XM23	M0003020 M0003030				
552	x12(1,1)=x1x2	MD003160				
553	X12(2,2)=X1Y2	M0003170				
554	x12(3,3)=x122	MDUD3180				
555	QD12=-(-R2*Q22*Q2*Q32-P2*Q42)*O.5	M0003370				
556	QD13=-(-R3*Q23+Q3*Q33-P3*Q43)*D.5	MD003380				
557	QD13=0.D					
558	QD21=-(R1*Q11-P1*Q31-Q1*Q41)*D.5	M0003390				
559	QD22=-(R2*Q12-P2*Q32-Q2*Q42)*0.5	MU00340				
560	QD23=-(R3+Q13-P3+Q33-Q3+Q43)+0.5	M000341				
561	0023=0.0					
562	0031=-(-01+011+P1+021-R1+041)+0.5	M0003420				
563 569	QD32=-(-Q2*Q12*P2*Q22-R2*Q42)*O.5	M0003430				
565	QD33=-(-Q3*Q13+P3*Q23-R3*Q43)*0.5 QD33=0.0	M0003440				
566	QD41=-(P1*Q11+Q1*Q21+R1*Q31)*0.5	M0003450				
567	Up42=-{P2*012+02*022+R2*032)*0.5	M0003450 M00 ₀ 3460				
568	QD43=-(P3*Q13+Q3*Q23+R3*Q33)*D.5	M0003460				
	THE TATE OF THE ACT TO THE STREET OF THE STR	110003410				

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570	7UO1 CONTINUE	M0003480				
571	61(1,1)=911**2 -921**2 -931**2 +941**2	MDDD3490				
72	61(1,2)=2.0*(011*021*031*041)	M0003500				
73	61(1,3)=2.0*(011*031-021*041)	M0003510				
74	G1(2,1)=2.0*(Q11*Q21-Q31*Q41)	M0003520				
75	61(2,2)=-011**2 +021**2 -031**2 +041**2	M0003530 ,				
76	61(2,3)=2.0*(021*031+011*041)	M0003540				
78	61(3,1)=2.6*(Q11*Q31+Q21*Q4 ₁) 61(3,2)=2.0*(Q21*Q31-Q11*Q41)	M0003550				
79	G1(3,3)=-011**2 -021**2 +Q31**2 +Q41**2					
80	7UO2 CONTINUE	M0003570 M0003580				
81	62(1,1) = 912**2 - 922**2 - 932**2 + 942**2	MDUD3590				
582	62(1,2)=2.0*(012*022+032*042)	M0003600				
583	62(1,3)=2.0+(912+932-922+942)	M0003610				
584	62(2,1)=2.0*(012*022-032*042)	MD003620				
565	6212,21=-012**2 +022**2 -032**2 +042**2	M000363n				
586	6212,31=2.0*1022*032+012*0421	M0003640				
587	62(3.1)=2.0*(012*032+022*042)	M0003650				
588	62(3,2)=2.0*(022*032-012*042)	MD003660				
589	62(3,3)=-012**2 -022**2 +032**2 +042**2	M0003670				
590	7003 CONTINUE	M0003680				
591	63(1,1)=013**2 -023**2 -033**2 +043**2	M0003690				
592	63(1,2)=2.0*(013*023*033*043)	M0003700				
93	63(1.3)=2.0*(913*933-923*943)	M0003710				
594	63(2,1)=2.0*(013*023-033*043)	M0003720				
595	6312.21=-013**2 +023**2 -033**2 +043**2	M0003730				
596	63(2,3)=2.0*(023*033*013*043)	M0003740				
597	63(3,1)=2.0*(013*033+023*043)	M0003750				
599	63(3,2)=2.0*(023*033-013*043) 63(3,3)=-013**2 -023**2 +033**2 +043**2	M0003760 M0003770				
600	7U04 CONTINUE	M0003770				
661	CALL HTXHPY(G2,G1,G12,3,-3,3)	MD003790				
602	CALL MTXMPY(63,61,613,3,-3,3)	M0003800				
603	DO 94 I=1,3	M0003810				
604	DO 94 J=1,3	M0003820				
605	B11(I,J)=G12(I,J)	M0003830				
606	B21(I,J)=G13(I,J)	M0U03840				
507	94 CONTINUE	M0003850				
FUP	DO 89 I=1,3	M0003860				
569	DO 89 J=1,3	MD003870				100
51C	G12(I,J)=-G12(I,J)	M0003880				
611	613(1,J)=-613(1,J)	M0003890				
612	89 CONTINUE	M0003900				
513	CALL MTXMPY(G12, XL1, B12, 3, 3, 3)	M0003910				
615	CALL MTXMPY(G13,XL2,B22,3,3,3) DO 95 I=1,3	MD003920 MD003930				
616	00 95 J=1,3	MD003930				
517	612(1,J)=-612(1,J)	MD003950				
18	613(1,J)=-613(1,J)	M0U03960				
19	95 CONTINUE	MD003760				
520	XOM1(1,1)=U.O	M0003980				
521	XOM1(1,2)=-R1	MDUD3990				
22	XOM1(1,3)=Q1	M0004000				
523	XOM1(2,1)=R1	M0004010				
24	XOM1(2,2)=0.0	M0004020				
25	X0M1(2,3)=-P1	M0004030				
626	XOM1(3,1)=-Q1	M0004040				

			,			
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627	XOM1(3,2)=P1	M0004050				
628	XOH1(3,3)=0.0	M0004060				
629	XOM2(1,1)=0.0	M0004070				
630	XOM2(1,2)=-R2	MO004080				
631	XOM2(1,3)=Q2	M0004090				
632	X0M2(2,1)=R2	M0004100				
633	X0M2(2,2)=0.0	M0004110				
639	X0M212.33=-P2 X0M2(3,1)=-Q2	M0004120 M0004130				
	X0M2(3,2)=P2	MO004130				
637	x0M2(3,3)=0.0	M0004150				
REPRODUC	X0M3(1,1)=0.0	M0004160				
₩ 639	x0m3(1,2)=-g3	MD004170				
9 640	XOM3(1,3)=Q3	M0004180				
641	X0H3(2.1)=R3	M0004190				
642	X0M3(2,2)=0.0	M0004200				
H 643	x0M3(2,3)=-P3	M0004210				
H 644	XOM3(3.1)=-Q3	M0004220				1684
REPRODUCIBILITY	X0M3(3,2)=P3	M0004230				
646	x0M3(3,3)=D.0	M0004240				
	00 88 1=1,3	M0004250				
	00 88 J=1,3	M0004260				
	XOM3(I,J)=-XOM3(I,J)	M0004270				
THE 652	88 CONTINUE	M0004280 M0004290				
OF 655 655 651 652	CALL MTXHPY(X0H2,612,AA,3,3,3)	H0004300				
653	CALL HTXMPY(612, XOM1, 88, 3, 3, 3)	H0004310				
654	00 81 1=1,3	MQ004320				
655	DO 81 J=1,3	M0004330				
656	BD11(I,J)=AA(I,J)+BB(I,J)	MD004340				
657	81 CONTINUE	M0004350				
658	CALL MTXMPY(XOM3,G13,AA,3,3,3)	MD004360				
659	CALL MTXMPY(G13,XOM1,BB,3,3,3)	M0004370				
660	D0 87 1=1,3	M0004380				
662	00 87 J=1,3	H00D4390				
663	BD21(I,J)=AA(I,J)+BB(I,J) 87 CONTINUE	M0004400				
664	00 82 1=1,3	M0004410 M0004420				
665	DO 82 J=1,3	M0004430				
666	BD11(I,J)=-BD11(I,J)	M0004440				
667	BD21(I,J)=-BD21(I,J)	M0004450			4	1000
668	82 CONTINUE	M0004460				
669	CALL MTXHPY(BD11, XL1, BD12, 3, 3, 3)	H0004470	SAT THE			
670	CALL MIXMPY(BD21, XL2, BD22, 3, 3, 3)	M0004480				
671	DO 8D I=1,3	M0004490				
672	DO 80 J=1,3	M0004500				
673	XOM2(I,J)=-XOM2(I,J)	M0004510				
674	x0M3(1,J)=-x0M3(1,J)	M0004520			7960	
675 676	BD11(I,J)=-BD11(I,J) BD21(I,J)=-BD21(I,J)	M0004530				
677	BU CONTINUE	M0004540				
678	DO 5 I=1,3	M0004550				
679	D0 5 J=1,3					
680	B(I,J)=B11(I,J)	MDUD458D				
681	BD(I,J)=BD11(I,J)	M0004590				
682	5 CONTINUE	M0004600				
683	DO 6 I=1.3	M0U04610				

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684	DO 6 J=4,6	M0004620				
685	8(1,J)=812(1,J-3)	M0004630				周围制
686	BD([,J)=BD12([,J-3)	M0004640				B. 174-25.0
667	6 CONTINUE	M0004650				
883	DO 11 I=4,6	HD004660				
689	00 11 J=1,3	M0004670				
69C	B(I,J)=821(I-3,J)	MD004680				
691	BD(I,J)=8021(I-3.J)	M0004690				
692	11 CONTINUE	M0004700				
693	DO 12 I=4,6	M0004710				
694	DO 12 J=4,6	M0004720				V
695	B(I,J)=B22(I-3,J-3)	M000473D				
696	BD(1,J)=BD22(1-3,J-3)	M0004740				
697	12 CONTINUE	M0004750				
698	XV1(1,1)=0.0	MD004760				
699	XY1(1,2)==W1	HD004770				
700	XV1(1,3)=V1	M0004780				
761	XV112.17=N1	M0004790				
762	XV1(2,2)=0.0	M0004800				
703	XV1(2,3)=-U1	M0004810				
704	xv1(3,1)=-v1	M0004820				
765	XV1(3,2)=U1	M0004830				
706	XV1(3,3)=0.0	M0004840				
767	XV2(1,1)=0.0	M0004850		87		
748	XV2(1,2)=-W2	M0004860				
769	XV2(1,3)=V2	M0004870				
710	XV2(2.1)=W2	M0004880				
711	XY2(2,2)=0.0	MOD04890				
713	XV2(2,3)=-02	M0004900				
714	xy2(3,1)=-y2 xy2(3,2)=u2	M0004910				
715	xv2(3,2)=0.0	MD004920				
716	XV3(1,1)=0.0	M0004930 M0004940				
717	XV3(1,2)=-N3	M0004950				
718	XV3(1,3)=V3	M0004960				
719	XV3(2,1)=W3	M0004970				
720	XV3(2,2)=0.0	M0004980				
721	xy3(2,3)=-U3	M0004990				
722	XV3(3,1)=-V3	M0005000				
723	XV3(3,2)=U3	M0005010				
724	XV3(3,3)=0.0	M0005020				
725	DO 83 I=1,3	M0005050				
726	DO 83 J=1,3	MD005060				
727	XOM1(I,J) = -XOM1(I,J)	M0005070				
728	83 CONTINUE	M0005080				
729	CALL MIXMPY(M1,XOH1,AA,3,3,3)					
730	CALL MTXMPY(AA,V1M,F11,3,3,1)	M0005040				
731	CALL MIXHPY (XOM1, XII, AA, 3, 3, 3)	M0005090				
732	CALL MTXMPY(AA,XOH11,XL11,3,3,1)	M0005100			Harage Waller	
733	00 37 1=1,3	M0005110				
734	0 ₀ 37 J=1,3	M0005120				-
735	XOM1(I,J) = -XOM1(I,J)	M0U05130				
736	XOM2(1,J)=-XOM2(1,J)					
737	37 CONTINUE	M0005140				
738	CALL MTXMPY(M2,XOM2,AA,3,3,3)					
739	CALL MIXMPY(AA, V2M, F2I, 3, 3, 1)	M0005160				
740	CALL MIXMPY (xOM2,x12,AA,3,3,3)	M0005210				

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741	CALL HTXMPY(AA, XOM21, XL21, 3, 3, 1)	M0U05220				
742	F21(1,1)=F21(1,1)+XHAPP+RAPP+(XOMD(11,1)+P2+R2)					
743	F2I(2,1)=F2I(2,1)+YMAPP*RAPP*(-XOMD(10,1)+Q2*R2)					
744	F21(3,1)=F21(3,1)+ZMAPP+RAPP+(-P2+P2-Q2+Q2)					
745	xL2I(1.1)=xL2I(1.1)+YMAPP*RAPP*(-XOMD(8,1)-U2*R2+W2*P2)					
746	XL2[(2,1)=xL2[(2,1)+xMAPP*RAPP*(+XOMD(7,1)+W2*Q2-V2*R2)					
747	00 28 1=1,3	MDU05230				
748	DO 28 J=1,3	M0005240				
749	x0M2(I,J)=-x0M2(I,J)	M0005250				
750	XOM3(I,J)=-XOM3(I,J)	M0005310				
751	28 CONTINUE	M0005260				
752	CALL MIXHPY(M3,XOM3,AA,3,3,3)					15591
753	CALL MTXHPY(AA,V3M,F3I,3,3,1)	M0005280				
754	CALL MIXMPY(XOM3,x13,AA,3,3,3)	M0005330				
755	CALL MIXMPY (AA, XOM 31, XL 31, 3, 3, 1)	M0005340				
756		M0005350				
757	DO 25 J=1,3	M0005360				
758	XOM3(I,J)=-XOM3(I,J)	M0005370				
759	25 CONTINUE	M0005380				
760	CALL MTXMPY(G1,XG1,FG1,3,3,1)	M0005390				
761	CALL MTXMPY(62, X62, F62, 3, 3, 1)	M0005400				
762	CALL MTXMPY(63, XG3, FG3, 3, 3, 1)	M0005410				,
763	7608 CONTINUE	M0005420				
769	CALL TBL(Z, ND, Z1, N1, UWD1)	M0005430				_
765	CALL TBL(Z,WD,ZZ,N1,UWDZ)	MD005440				
766	C NEXT 2 CARDS ZERO OUT THE WINDS					-
767	UWD1=0.0					
768	UMDS=0+0	M0005450				-
769	WVD1=0.0	H0005460				
770	WWD2=0+0	M0005470				
771	WWD3=0.0 VWD1=UWD1	M0005480				
773	VWD3=UWD2	M0005510				-
774		M0005520				
775	WIN1(1,1)=UWD1 WIN1(2,1)=VWD1	M0005530				
776	WIN1(3,1)=WWD1	M0005540				
777	7UD9 CONTINUE	M0005550				_
778	CALL MTXMPY(G1, WIN1, WIN1, 3, 3, 1)	M0005560				
779	UWD1=WIN1(1.1)	M0005570				
780	VWD1=WIN1(2,1)	MDD05580				
781	WWD1=WIN1(3,1)	M0005590				
782	WIN2(1,1)=UWD2	M0005600				
783	WIN2(2,1)=VWD2	M0005610				
784	wIN2(3,1)=wwD2	M0005620				
785	7JID CONTINUE	M0005630				
786	CALL MIXMPY (G2, WIN2, WIN2, 3, 3, 1)	HD005640				
787	UMD2=WIN2(1,1)	MD005650				
788	VWD2=WIN2(2,1)	MD005660				
789	WWD2=WIN2(3,1)	M0005670				
796	WIN3(1,1)=UWD3	MD005680				
791	WIN3(2,1)=VWD3	M0005690				
792	WIN3(3,1)=WWD3	H0005700				
793	7G11 CONTINUE	M0005710				
794	CALL MTXMPY(G3,WIN3,WIN3,3,3,1)	M0005720				
795	UWD3=WIN3(1,1)	M0U0573U				
173						
796	VWD3=WIN3(2,1)	MOU05740				

4						
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798	7u12 CONTINUE	M0005760				
799	UH1=U1-UWD1	H0005770				
800	UH2=U2-UND2-RALPHA+Q2					
801	UH3=U3-UWD3	M0005790				
802	VH1=V1-VWD1	M0005800				
803	VH2=V2-VWD2+RALPHA+P2					
864	VH3=V3-VWD3					
REPROD	NH1=N1-WWD1	M0005830				
西 806	NH2=N2-UND2	M0005840				
E 867	WH3=W3-WWD3	M0005850				
808	V11=(UH1+UH1+VH1+VH1+WH1+WH1)++D.5	M0005860				
809	V21=(UH2*UH2+VH2*VH2*WH2*WH2)**0.5	M0005870				
REPRODUCIBILITY 816 817 817 818 817 818 817 818 818	V31=(UH3+UH3+VH3+VH3+WH3)**O.5	M0005880				
G 811	VSQUND=0.0037*Z1+1138.0	Hoppasson				
BH 813 814 815	MACH1=V11/VSQUND					
H 813	AL1=ARGOS(NH1/V111+57.3					
E 819	AL2=ARCOS(NH2/V21)+57.3					
815	AL3=ARCQS(NH3/V31)*57.3					
₩ 816	7613 CONTINUE	нооо5950				
	CALL TBLND(-1,3,ZCNA,XMAAL,NAZ,ZXA,NSZ,CNA1)	HUUU373U				
9 817	CALL TBLND(-1,3.ZCMA,XMAAL,NAZ,ZXA,NSZ,CMA1)					
	CALL TBLND(-1,3,2CAA, XHAAL, NAZ, ZXA, NSZ, CAA1)					
H 819 118 820	CMA1=CMA1+CNA1+(ZMRP1/YL)					
H 820 E 821	CALL TBLND(-1,3,ZCNA2,PERALZ,NAZZ,ZXAZ,NSZZ,CNAZ)					
822	CALL TBLND(-1,3,2CHA2,PERAL2,NAZ2,ZXA2,NSZ2,CMA2)					
823	CALL TBLND1-1.3.ZCAAZ,PERALZ,NAZZ,ZXAZ,NSZZ,CAAZ)					
824	CHAZ=CMAZ+CNAZ*(ZMRPZ/YPL)					
825	CALL TBL (AL, FCNA3, AL3, N, CNA3)					
826	CALL TBLIAL, FCAA3, AL3, N, CAA3)					
827	CALL TBL (AL, FCHA3, AL3, N, CHA3)					
828	7014 CONTINUE	MD006200				
829	QA1 = 0.5*RH0*V11*V11*S1	MD006210				
830	QBAR1=QA1/S1	MUUUULIU				
831	QA2=0.5*RH0*y21*y21*ST2					
832	QBAR2=QA2/ST2					
833	4A3=D.5*RHO*Y31*Y31*S3					
834	UVG1=(UH1*UH1+VH1*VH1)**0.5					
835	UVGZ=(UH2*UH2+VH2*VH2)**D.5					
836	UVG3=(UH3+UH3+VH3+VH3)**0.5					
837	Fx1=-QA1*CNA1*(UH1/UVG1)					
838	FX2=-QA2+CNA2+(UH2/UVG2)					
839	FX3=-QA3+CNA3+(UH3/UVG3)					
840	FY1=-QA1+CNA1+(VH1/UVG1)					
841	FY2=-QA2*CNA2*(VH2/UVG2)					
842	FY3=-QA3+CNA3+(VH3/UVG3)					
843	FZ1=-QA1+CAA1					
844	FZ2=-QAZ+CAAZ-MZDOT+WZ					
845	FZ3=-QA3+CAA3					
846	YL1=QA1+YL+CMA1+(VH1/UVG1)					
847	YL2=QA2*YPL*CHA2*(YH2/UVG2)					
848	YL3=QA3*YPL3*CMA3*(VH3/UVG3)					
849	YM1=-QA1+YL+CMA1+(UH1/UVG1)					
850	YM2=-QA2+YPL+CMA2+(UH2/UVG2)					
851	YH3=-QA3+YPL3+CHA3+(UH3/UVG3)					
852	YN1=0.0					
853	YN2=Q.0					
ACCORDING TO A LOCAL CONTROL OF THE OWNER, T						

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855	7016 CONTINUE	M0006430				
856	CALL MTXMPY(8,MI,AIA,6,18,18)	MD006440				
857	CALL MTXMPY(AIA.B.K.6,-18,6)	M0006450				
858	00 501 1=1,6	M0006460				
859	DO 501 J=1,6	M0006470				
860	KINV(I,J)=0.0	M0006480				
861	501 CONTINUE	M0006490				
862	KINV(1,1)=1.0	MQ006500				
863	KINV(2,2)=1.0	M0006510				
864	KINY(3,3)=1.0	M0006520				
865	KINV(4,4)=1.0	M0006530				
866	KINV(5,5)=1.0	M0006540				
868	KINV(6,6)=1.0 CALL LINSYS(K:6:6:DET:KINV:6)	M0006550				
869	DO 701 I=1,6	M0006560 M0006570				
870	DO 701 J=1.18	M0006580				
871	B(1,J)=-B(1,J)	M0006590				
872	701 CONTINUE	M0006600				
873	CALL HTXMPY (B.KINV, BIB, -18, 6, 6)	M0006610				
874	00 703 I=1,6	M0006620				
875	00 703 J=1.18	MD006630				
876	B(I,J)=-B(I,J)	MDDD6640				
817	7n3 CONTINUE	M0006650				
878	CALL HTXMPY(BIB,BD,T2,18,6,18)	M0006660				
879	CALL MTXHPY(BIB,AIA,T1,18,6,18)	M0006670			Street Malerine	
880	CALL TBL(TIMX.THR.TIME.NZ.THR1)					
881	FC(1,1)=THR1+CP1+RETR					
882	FC(2,1)=THR1+CP2+RETR					
883	FC(3,1)=THR1+CP3+RETR					
884	FC(4,1)=THR1*CP4*RETR					
885	FC(5,1)=THR1*CP5*RETR					
886	FC(6.1)=THR1*CP6*RETR					
887	DO 502 I=1,18	MD006680				
888		M0006690				
889	FS(I,J)=FI(I,J)+FA(I,J)+FG(I,J)+FC(I,J)	M0006700				
890	502 CONTINUE	M0006710				
891	CALL MTXMPY(T1,FS,FR1,18,18,1)	M0006720				
893	CALL MTXHPY(T2,XOM,FR2,18,18,1) DO 503 I=1,18	M0006730				
894	J=1	M0006740 M0006750				
895	FR(I,J)=FR1(I,J)+FR2(I,J)	M0006760				
896	5D3 CONTINUE	M0006770				
897	DO 504 I=1,18	M0006780				
P98	J=1	M0006790				
899	FS1(1,J)=F1(1,J)+FR(1,J)+FA(1,J)+FG(1,J)+FC(1,J)	M0006800				
900	504 CONTINUE	MD006810				
901	CALL MTXMPY(MI,FS1,XOMD,18,18,1)	M0006820				
912	C THE NEXT 3 CARDS ZERO OUT XOMD FOR THE 2ND PARACHUTE					
953	XOMD(13,1)=0.0		and delining			
934	XOMD(14,1)=0.0					
905	X0MD(15,1)=0.0					
906	CALL MIXMPY (AIA.KINV. BB1, -18,6,6)					
967	CALL MTXMPY(BB1,B,CC1,18,6,18)					
968	CALL MTXMPY(CC1,XOM,XOHC,18,18,1)					
909	DO 9019 I=1,18					
910	J=1					
911	XOM(I,J)=XOM(I,J)-XOMC(I,J)					

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35	ñ	٠		
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112	9019 CONTINUE					
13	T = TIME'	M0006830				
11.	DO 3001 I=1,18					
15	DO 3001 J=1,18	M0006870				
16	XOHT(1,J)=0:0	M0006880				
17	3UO1 CONTINUE	M0006890				
16	DO 3002 1=1,3	M0006900				
19	00 3002 J=1,3	M0006910				
50	XOMT(1,J)=G1(J,I)	M0006920				
21	XOMI(1+6,J+6)=G2(J,1)	M0006930				
22	XOMT(I+12,J+12)=63(J,I)	MDDD6950				
23	3DDZ CONTINUE	M0006960				
24	CALL HTXMPY (XOMT, XOM, XOMF, 18, 18, 1)	110000900				
25	X1D=X0MF(1 :1) Y1D=X0MF(2 :1)					
26 27	경영하실 BB (CC) (Fig. 1) : [1] [1] [1] [1] [1] [2] [2] [3] [3] [4] [4] [4] [4] [4] [4] [4] [4] [4] [4					
28	Z1D=X0MF(3 -1) X2D=X0MF(7 -1)					
49	Y2D=X0MF(8 11					
30	22D_XOMF (9 .1)					
31	x3D=X0HF(13,1)					
32	Y3D=X0MF(14,1)					
33	Z30=X0MF(15,1)					
734	IND=IND+1	M0006840				
35	IF (IND-41500,500,600	M0006850				
36	-600 CONTINUE					
37	DIRC=ARCOS(G1(3,3))*57.3					
38	SSS1=(1-(G1(1,3)*G1(1,3)))**0.5					
39	SSS2=(1-(62(1,3)*62(1,3)))**0.5					
40	SSS3=(1-(G3(1,3)*G3(1,3))**0.5					
41	THI1=XTAN2(-G1(1,3),SSS1)					
42	TH12=XTAN2(-G2(1,3),SSS2)					
43	TH13=XTAN2(-G3(1,3),SSS3)					
44	PHI1=XTAN2(61(2,3),61(3,3))					
45	PHI2=XTAN2(G2(2,3),G2(3,3))					
46	PHI3=XTAN2(G3(2,3),G3(3,3)) PSI1=XTAN2(G1(1,2),G1(1,1))					
48	PSI2=XTAN2(G2(1,2),G2(1,1))					
149	PSI3=XTAN2(G3(1,2),G3(1,1))					
50	IF(T-TPR)4006,7006,7006					
51	7406 PRINT 1000,T	MD007180				
52	TPR=TPR+DELP					
53	1000 FORMAT (1H0,4HTIME,3X,E15.6)	M0007190				
54	PRINT 6666,DIRC					
155	6666 FORMAT (1H, 4HDIRC, 3X, F15.6)					
756	PRINT 9898, (CMA1, CMA1)					
57	PRINT 9899, (CMA2, CNA2, CAA2)					
58	9898 FORMAT (1H,4HCMA1,3X,E15.6,2X,4HCNA1,3X,E15.6,2X,4HCAA1,3X,E15.6)					
159	9899 FORMAT (1H,4HCMA2,3x,E15.6,2x,4HCNA2,3x,E15.6,2x,4HCAA2,3x,E15.6)					
396	PRINT 7050	M0007200				
761	705g FORMAT 118,2HFA,125,2HFI,140,2HFG,155,2HFR,170,4HDOMG,185 ,3HOMG,	M0007210				
962	17100,2HFC,//)					
763	PRINT 7051, (FA(I,1),FI(I,1),FG(I,1),FR(I,1),XOMD(I,1),XOM(I,1),	M0007230				
764	1fC(I,1),I=1,18)					
765	7551 FORMAT (7E15.8)	M0U07250				
166	PRINT 1001, (X1, Y1, Z1, THI1, PHI1, PSI1)					
67	IUC1 FORMAT (1H +	M0007270				

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969	13X,E15.6,2X,4HPH11,3X,E15.6,2X,4HPST1,3X,E15.6)	M0007290				
970	PRINT 1002, (U1.V1.V1.P1.Q1.R1)	M0007300				
971	1UD2 FORMAT (1H ,	M0007310				
972	1 2HU1, 3X, E15.6, 2X, 2HV1, 3x, E15.6, 2X, 2HW1, 3X, E15.6/2	X,2HP1,3XMOOD7320				
973	1,E15.6,2X,2HQ1,3X,E15.6,2X,2HR1,3X,E15.6)	M0007330				
974	PRINT 1003.(AL1)					
975	1003 FORMAT (1H ,	M0007350				
976	1 3HAL1,3X,E15.6)					
977	PRINT 6001, (x2, y2, Z2, THI2, PHI2, PSI2)					
Q 2 978	6UO1 FORMAT (1H .	M0007390				
978 979 979 981 982 982 983 983 983	1 2HX2,3X,E15.6,2X,2HY2,3X,E15.6,2X,2H22,3X,E15.6/2	x,4HTH12,M0007400				
Q 3 980	13X,E15.6,2X,4HPHI2,3X,E15.6,2X,4HPSI2,3X,E15.6)	H0007410				
70 981	PRINT 6002, (U2, V2, W2, P2, Q2, R2)	MD007420				
978 979 980 981 982 982 982 983	6LO2 FORMAT (1H ,	M0007430				
G 983	1 2HU2,3x,E15.6,2x,2HV2,3x,E15.6,2x,2HW2,3x,E15.6/2					
_Ω 989	1,E15,6,2X,2H02,3X,E15,6,2X,2HR2,3x,E15,6)	M00 ₀ 7450				
	PRINT 6003, (AL2)					
AGE 786	6UD3 FORMAT (1H .	M0007470				
H 1 987	1 3HAL2,3X,E15.6)					
- 298R	PRINT 1010, (RHO,QBAR2,QBAR1)					
55 989	1010 FORMAT (1H, 3HRHO, 3X, E15.6, 2X, 5HQBAR2, 3X, E15.6, 2X, 5HQBAR1,	3x,E15.6)				
P 9990	HXB=XIX1*P1					
PO 1992	HYB=XIY1*Q1					
Ø ⊨392	HZB=XIZ ₁ *R ₁					
₩ II 993	HXI=G1(1,1)*HXB+G1(2,1)*HYB+G1(3,1)*HZB					
€994	HYI=G1(1,2)+HXB+G1(2,2)+HYB+G1(3,2)+HZB					
995	HZI=G1(1,3)+HXB+G1(2,3)+HYB+G1(3,3)+HZB					
996	TAM=SQRT(HXI+HXI+HYI+HYI+HZI+HZI)					
997	PRINT 9304, (TAM, HXI, HYI, HZI)					
998	9304 FORMAT (1H, 3HTAM, 3X, E15.6, 2X, 3HHXI, 3X, E15.6, 2X, 3HHYI, 3X, E	15.6,2X,				
999	13HHZI,3X,E15.6)					
1000	6169 FORMAT (16E12.6) .					
	1111 FORMAT (11H, 2HS2, 3X, E15.6)					
1002	PRINT 1111,52 NM=NM+1					
1003						
1005	PTIME (NM)=TIME					
1006	PZ1(NM)=Z1 PFR7(NM)=FR(7,1)					
1667	PFR8(NM)=FR(8,1)					
1008	PFR9(NM)=FR(9,1)					
1009	PS2(NM)=S2					
1010	PQBAR1(NM)=QBAR1					
1011	PQBAR2(NH)=QBAR2					
1012	PP1(NM)=P1*57.3					
1013	PQ1(NH)=Q1+57.3					
1014	PR1(NM)=R1*57.3					
1015	PZ2 (NM)=Z2					
1016	PDX1(NM)=XOMF(1,1)					
1017	PDY1(NH)=XOMF(2,1)					
1018	PDZ1(NM)=XOMF(3,1)					
1019	PALI(NM)=AL1					
1020	PAL2(NM)=AL2					
1021	IF(TIME-20.0)4006,9001,9001					
1022	4006 11=11+1	M0007510				
1023	60 10 200	M0007520				0.000
1024	9UO1 CONTINUE					
1025	CALL IDENT 19,9HCUT PAPER)					

MAIN			DATE	040379	PAGE	. 15
1026	CALL QUIK3V (-1,35,TIMEL,ZIL,-NM,PTIME,PZI)					
1027	CALL QUIK3V (-1.35.TIMEL.PFRL7NM.PTIME.PFR7)					
028	CALL QUIK3V (-1,35,TIMEL,PFRL8,-NM,PTIHE,PFR8)					
029	CALL QUIKSV (-1,35 TIMEL, PFRL9, -NM, PTIME, PFR9)					
030	CALL QUIKSV 1-1,35,TIMEL,PS2L ,-NM,PTIME,PS2)					
031	CALL QUIKSV (-1,35,TIMEL,POBALL,-NM,PTIME,PQBAR1)					
032	CALL QUIK3V (-1,35,TIMEL,PQBA2L,-NM,PTIME,PQBAR2)					
033	CALL QUIKSY (-1,35.TIMEL.PZZLNM.PTIME.PZZ)					
034	CALL QUIKSV (-1,35,TIMEL,PP1L,-NM,PTIME,PP1)					
035	CALL QUIKSY (-1,35,TIMEL,PQ1L,-NM,PTIME,PQ1)					
036	CALL QUIKSV (-1,35,TIMEL,PRIL,-NH,PTIME,PRI)					
037 038	CALL QUIK3V (-1.35.TIMEL.PDX1LNM.PTIME.PDX1) CALL QUIK3V (-1.35.TIMEL.PDY1L,-NM.PTIME.PDY1)					
039	CALL QUIK3V (-1.35.TIMEL.PDZILNM.PTIME.PDZI)					
040	CALL QUIKSV (-1,35,TIMEL,PALIL,-NM,PTIME,PALI)					
041	CALL QUINSV (-1,35,TIMEL, PALZL, -NM, PTIME, PALZ)					
042	CALL ENDJOB					
043	CALL EXIT					
CHA	9101 CONTINUE					
045	END	M0007540				
G,P	RUNGE					
	AND A THERE A VALUE	THE LONG LABOR.				
		TELEFICIAL PROPERTY OF THE PERSON NAMED IN COLUMN TO THE PERSON NA				
		1911 Sp. (1912 LEAD 188)				
		50 DE 1810				
	The state of the s					

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MUDPHYBIN2U6*TPF$(U).RUNGE
                   SUBROUTINE RUNGE (KUTTA.TIME.DT.NVAR.NDVAR)
               KUTTA IS A CONTROL INTEGER
            C TIME IS TIME OF INTEGRATION
            C DT IS THE TIME INCREMENT
               NVAR = NUMBER OF VARIABLES TO BE INTEGRATED ONCE
     6
            C NOVAR = NUMBER OF VARIABLES TO BE INTEGRATED THICE
     7
                  DIMENSION C1( 60), C2( 60), C3( 60), C4( 60), CD1( 60), CD2( 60),
                  1 CD3( 60) CD4( 60), SX( 60), SXD( 60)
     8
     9
                  COMMON/FUNT/ x( 60)
    10
                  COMMON/FIRT/ XDI 601
    11
                   COMMON/SECD/XDD(30)
    12
                   GO TO (1.2.3.4) . KUTTA
    13
                1 DO 10 1=1.NYAR
    14
                   SX(1) = X(1)
    15
                   C1(1) = xD(1)+DT
    16
               10 x(1) = $x(1)+0.5*C1(1)
                   IF (NoVAR.EQ.D)GO TO 50
    17
    18
                  DO 100 I=1.NOVAR
    19
                   SXD(I) = XD(I)
    20
                   CD1(I) = XDD(I)*DT
    21
              100 XD(I) = SXD(I)+0.5*CD1(I)
    22
                  CONTINUE
                  TIME = TIME + D.5+DT
    23
    24
                  RETURN
    25
                2 00 20 I=1.NVAR
    26
                   C2(1) = XD(1)*DT
    27
               20 x(1) = Sx(1)+0.5*C2(1)
    28
                  IF INDVAR.EQ.DIGO TO 51
    29
                  DO 200 I=1,NOVAR
    30
                  CD2(I) = XDD(I)*DT
    31
              200 xp(1) = SxD(1)+0.5*CD2(1)
    32
                  CONTINUE
    33
                  RETURN
    34
                3 DO 3n I=1.NVAR
    35
                  C3(1) = XD(1)*DT
    36
               30 x(1) = SX(1)+C3(1)
    37
                  IF (NDVAR.EQ.D) GO TO 52
    38
                  DO 300 I=1.NDVAR
    39
                  CD3(I) = XDD(I)*DT
    40
              306 XD(1) = SXD(1)+CD3(1)
    41
             52 CONTINUE
    42
                  TIME = TIME+0.5*DT
    43
                  RETURN
    44
                4 DO 40 I=1.NVAR
    45
                  C4(I) = XD(I)*DT
    46
               40 X(1) = SX(1)+(C1(1)+C4(1)+2.*(C2(1)+C3(1)))/6.0
    47
                  IF (NDVAR.EQ.D)GO TO 53
   48
                  DO 400 I=1.NDVAR
   49
                  CD4(I) = XDD(I)+DT
              400 xD(I) = SXD(I)+(CD1(I)+CD4(I)+2.0+(CD2(I)+CD3(I)))/6.0
   SC.
   51
                  CONTINUE
   52
                  RETURN
   53
                  END
```

TBL		DATE 040379 PAGE 2
	IN2U6+TPF\$(U).TBL	
1	SUBROUTINE TBL(X,Y,X1,N,Y1)	
2	C THE DATA MUST BE IN ASCENDING ORDER	
. 3	DIMENSION X(1),Y(1)	
•	DO 93 I=1,N	
5	1F(X(1)-X1)93,95,91	
6	91 Dx=x1-x(I-1)	
_7	DX1=X(I)=X(I=1)	
8	DA=A(1)-A(1-1)	
9	Y1=Y(1-1)+DY+(0X/DX1)	
10	60 10 94	
11	95 Y1=Y(1)	
12	60 10 94	
13	93 CONTINUE	
15	94 CONTINUE	
16	RETURN END	
16	END	
4H06,P	TBLND	
apri,s	1BLND	
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TBLND						DATE	040379	PAGE	
JRPHYBINZE6	*TPF\$(U).TBLND								
1		TBL ND (NEXTR. ND. Z. X. NA. XA. NS. ANS)							
네 일 좀 많은 하다 하는데 얼마를 다 하는데 다 그렇게 나 없었다.	C				TBLN0010				
3	C N-DIMENSIONAL	TABLE LOOK-UP ROUTINE	03	/20/73	TBLN0020				
	C				TBLN0030				
A CONTRACT OF THE PARTY OF THE	С				TBLN0060				
6	C				TBLN0070				
	C				TBLN0080				
8	C NEXTR	EXTRAPOLATION CONTROL CINTEGER			TBLN0090				
9	C	IF ZERO. NO EXTRAPOLATION ERUN	TERMINATED		IBLN0100				
10	C	IF POSITIVE, EXTRAPOLATION OCC			TBLN0110				
4 11	C	IF NEGATIVE. NO EXTRAPOLATION	TO THE PROPERTY OF THE PROPERT	COLUMN TO THE PARTY OF THE PART	TBLN0120				
12	C ND	TABLE LOOK-UP DIMENSION, LIMITED			TBLN0130				
Z 13	C	LONE GREATER THAN NUMBER OF INDEP			TBLN0140				
214	C	IF POSITIVE, INDEPENDENT VECTO			TBLN0150				
215	6	IF NEGATIVE . SAVED VALUES OF I	NDEPENDENT VE	CTOR	IBLN0160				
3 16	C	INDICES ARE USED			TBLN0170				
¥ 1.7	C Z	TABLE OF DEPENDENT PARAMETERS CRE	AL ARRAYJ		IBLN0180				
22 18	C X	TABLE OF INDEPENDENT VECTORS CREA			TBLND190				
19	¢	LEACH VECTOR MUST BE IN ASCENDING	ORDER		TBLNOZOO				
326	C	EXAMPLE OF X AND Z TABLESE			TBLN0210				
	C	X-TABLE Z-TAB			TBLND220				
12	C	Al Cl,C4 FOR			TBLN0230				
9 23	C	A2 8 8	B2 0 0		TBLN0240				
	C	81 a a	B3 8 8		TBLN0250				
25	C	B2 8 0	B1 9 A2		TBLN0260				
25 26 27	C	83 a a	B2 a a		TBLN0270				
	C	C1 a a	B3 a a		TBLN0280				
28	C	C2			TBLN0290				
29	C	C3			TBLN0300				
30	C	C4			TBLN0310				
31	C NA	LENGTH OF EACH INDEPENDENT VECTOR	CINTEGER ARR	AYJ	IBLN0320				
32	C	EXAMPLES NAC33 > 2, 3, 4			TBLN0330				
33	C XA	INDEPENDENT PARAMETERS CREAL ARRA			TBLN0340				
34	C NS	SAVED VALUES OF INDEPENDENT VECTO			TBLN0350				
35	C	ESHOULD BE INITIALLY SET TO -1 SO	Contraction of the Contraction o	DENT	TBLN0360				
	C	VECTORS ARE TESTED FOR ASCENDI	NG ORDER J		TBLN0370				
	C				TBLN0380				
38					TBLN0390				
39	C ERROR COND	la da Indiana antiga de la mala de marcha de la marcha de la marcha de la filia de la calenda de la marcha de		NIED	TBLN0400				
	C	AND THE RUN IS TERMINAT			TBLN0410				
THE THE PROPERTY OF THE PARTY OF THE PARTY.		EAST ONE OF THE INDEPENDENT VECTO	RS 15 NOT IN		TBLN0420				
		NDING ORDER.		NOFN*	TBLN0430				
43		NEXTR SET TO ZERO, AT LEAST ONE			TBLN0440				
48		METERS IS OUT OF RANGE OF THE IND		OK2.	TBLN0450				
	5. TABI	E LOOK-UP DIMENSION, ND, IS GREAT	EK IHAN DO		TBLN0460				
46	C				TBLND470 TBLNO480				
47	DIMENATON	7411 W411 NA41, VA411 NC411							
48	DIMENSION	Z(1), X(1), NA(1), XA(1), NS(1), RATIO(5), NGROUP(5), ITOT(5), WJ(721		0490				
49 50	c ·	WELTGEST WORDOLEST TIOLEST MAC	36)		U500 TBLN0510				
					TBLN0560				
	C				TBLN0600				
52									
THE STREET STREET, SHOWING STREET, STR	1 15 (ND 17	03 60 70 40			TBLN0610				
59		0) 60 10 60			0620				
55	2 WRITE (6,9)	7) 60 70 10			0630 0640				

1BLND		DATE	040379	PAGE	2	
57	4 WRITE (6,904)	0650				
58	C STOP	0660 18LN0670				
59 60	10 L1 = 1	0680				
61	LF = ND - 1	0690				
62	DO 39 I=1•LF	0700				
63	L2 = L1 + NA(I) = 1	0710				
64	IF (NS(I) .GT1) GO TO 20	0720				
5	NS(I) = 0	0730				
66	JF = L2 - 1	0740				
67	DO 12 J=L1,JF	0750				
8	1F (X(J) .LT. X(J+1)) 60 TO 12	0760				
69	11 WRITE (6,902)	0770				
70	WRITE (6,911) 1. J	0780				
71	60 10 90	0790				
12	12 CONTINUE	0800				
13	С	TBLN0810				
9	20 IF (NS(I) .LT. L1 .OR. NS(I) .GT. L2) NS(I) = L1 - 1	0820				
15	IF (XA(I) .GT. X(L1) .AND. XA(I) .LT. X(L2)) GO TO 22	0830				
16	IF (XA(I) *GE* X(L2)) NS(I) = L2 IF (XA(I) *LE* X(L1)) NS(I) = L1 - 1	0840 0850				
18	21 IF (NEXIR) 33.30.32	0860				
9	22 IF (NS(I) .EQ. [2) NS(I) = L2 - 1	0870				
0	L = NS(I)	0880				
1	LL = 1	0890				
12	IF (L .LT. L1) 60 TO 26	0900				
13	IF (XA(I) .LE. X(L)) LL = -1	0910				
84	29 IF (XA(I) .GT. X(L) .AND. XA(I) .LE. X(L+1)) GO TO 33	0920				
85	26 L = L + LL	0930				
86	NS(I) = L	0940			n 18 11 5	
87	IF (L .GE. L1 .AND. L .LT. L2) GO TO 24	0950				
86	60 TO 21	0960				
89	30 WRITE (6,902)	0970				
90	WRITE (6,930) I	0980				
1	60 TO 90	0990				
3	32 IF (NS(I) •GE, L2) NS(I) = L2 - 1 IF (NS(I) •L7 • L1) NS(I) = L1	1000				
•	C (W2(1) *F1* (1) W2(1) = F1	1010 TBLN1020				
5	33 KA = NS(I)	1030				
6	KB = NS(I) + 1	1040				
7	IF (NS(I) .LT. L1) KA = L1	1050				
8	IF (NS(I) .EQ. L2) KB = L2	1060				
9	1F (X(KA) .EQ. X(KB)) GO TO 35	1070				
00	34 RATIO(1) = (XA(1) - X(KA)) / (X(KB) - X(KA))	1080				
.1	60 10 37	1090				
12	35 RATIO(1) = 0.0	1100				
,3	NS(I) = KA	1110				
14	37 L1 = L2 + 1	1120				
15	39 CONTINUE	1130				
6	C LORONINALI - MEZIL	TBLN1140				
7	46 NGROUP(1) = NS(1)	1150				
16	NSUH = NA(1)	1160				
10	42 DO 44 I=2,LF NGROUP(I) = NS(I) - NSUM	1170				
		1180				
2	NSUM = NSUM + NA(I) 44 CONTINUE	1190				
3	1707(LF) = 1	1200				

TBLND			DATE 040379	PAGE	3
114	C	TBLN1220			
115	50 D0 52 I=2,LF	1230			
116	J=LF-1+1				
117	ITOT(J) = ITOT(J+1) + MA(J+1)	1250			
118	52 CONTINUE	1260			
119	C	TBLN1270			
120	60 KF = 200LF	1280			
1 21	Mw = -2	1290			
REPRODUCIBILITY OF	61 DO 69 1=1.KF,2	1300			
23	IFIRST = 1	1310			
Z 24	Mw = MW + 2	1320			
225	62 DO 67 J=1, LF				
26	MM = 2**(J=1)	1340			
G27	- NHB = MH				
H 28	MAN = MM				ALEXANDE.
H 29	CALL BIN(MMM.D.36.p.mWM.1)				
13F	1F (MMM.EQ.D) GO TO 65				
1 1	IMON = NGROUP(J) + 1	1360			
19 2	60 10 66	1370			
03	65 IMON = NGROUP(J)	1380			
6 3°	66 IFIRST = IFIRST + (IMON-1)*ITOT(J)	1390			Alexander
135 138	67 CONTINUE	1400			
95	ISEC = IFIRST + ITOT(1)	1410			
1 7	WJ(I) = Z(IFIRST)	1420			ALC: N
138	WJ(I+1) = Z(ISEC)	1430			
139	69 CONTINUE	1440			
140		TBLN1450			
141	7C 00 79 I=1,LF	1460			
142	KF = KF/2	1470			
143	71 DO 77 J=1,KF	1480			
144	MJ(J) = MJ(2*J-1)	1490			
145	IF (RATIO(I) .EQ. 0.0) GO TO 77	1500			
147	WJ(J) = WJ(J) + (WJ(2*J) - WJ(2*J-1)) * RATIO(1) 77 CONTINUE	1510			
148	79 CONTINUE	1520			
149	17 CONTINUE	1530 TBLN1540			
150	8C ANS = HJ(1)	IDENTIAN			
151	RETURN	1560			
152		TBLN1570			
153	90 CONTINUE	TOURISTO			
154	RETURN	1600			
155	c	TBLN1610			
156	902 FORMAT (1H1/10X, "ERROR OCCURRED IN TBLND ROUTINE"/1H 1	1620			
157	904 FORMAT (10x. DIMENSION OF TABLE EXCEEDS 6 (M = ".12.")")	1630			
158	911 FORMAT (10x, "INDEPENDENT VECTOR NO. ", 12, " IS NOT IN ASCEND	ING ORD 1640			
159	*ER AT INDEX NO. 13)	1650			
160	930 FORMAT (10x, "INDEPENDENT PARAMETER NO. ",12," IS OUT OF RANGE				
161	*HE CORRESPONDING VECTOR (K = D)*)	1670			
162	10u00 CONTINUE				
163	E.ND	1680			

aHDG,P XTAN2

OPRI,S X1AN2 FURPUR 27F3DE33 SL73R1 04/03/79 18:29:36

XTAN2			DATE 040379 PAGE 1
	GA+TPFS(L).XTAN2		
1	FUNCTION XTAN2(A.B) IF(B .EQ. O.O) GO TO 100 XTAN2=ATAN2(A.B)+57.3 RETURN		
2	IF (B .EQ. D.D) 60 TO 100	F**	
:	DETUDN		
5	100 IF (A) 10-16-15	F.C. X-	
6	10 XTAN2=-90.0	161	
	RETURN		
6	16 XTAN2=0.0	1.7.	
9	15 XTAN2=90.0		
11	RETURN		
17	END		
•			
	· · · · · · · · · · · · · · · · · · ·		

APPROVAL

COMPUTER PROGRAM DEVELOPMENT AND USER'S MANUAL FOR PROGRAM PARACH

by Hughlen I. Murphree

The information in this report has been reviewed for security classification. Review of any information concerning Department of Defense or Atomic Energy Commission programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

This document has also been reviewed and approved for technical accuracy.

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